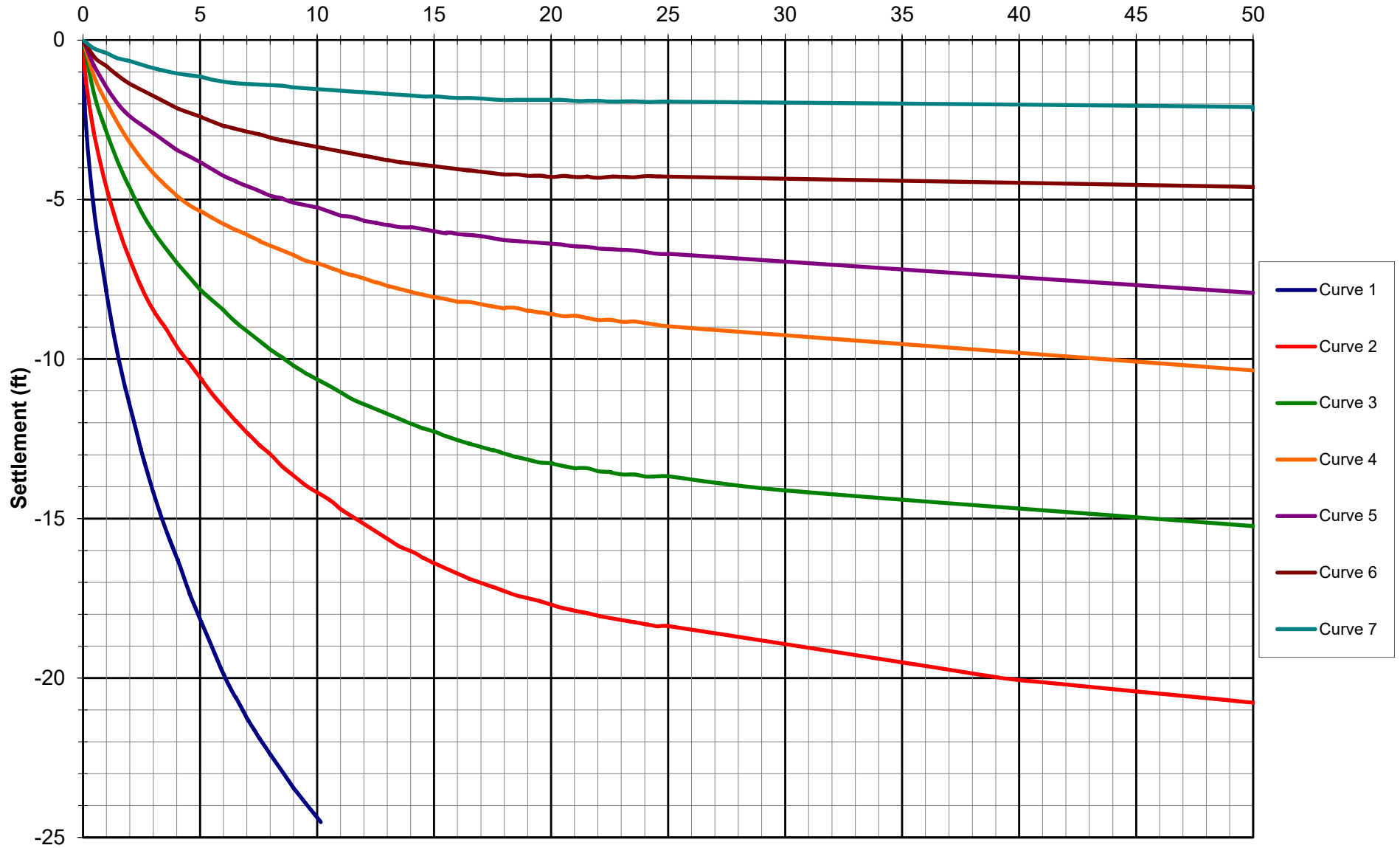
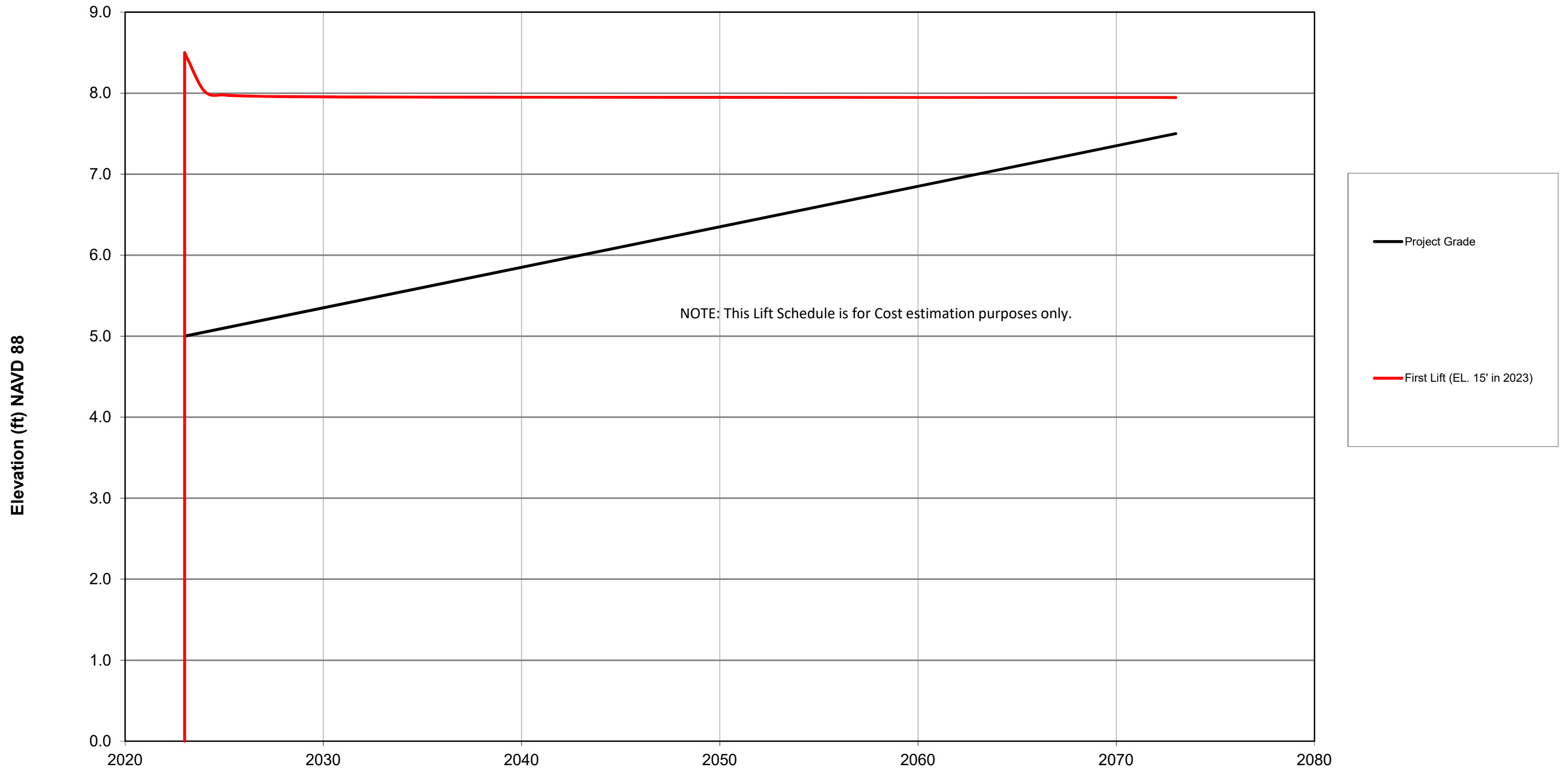


# Upper Barataria Basin, LA - Feasibility Study Settlement - USACE Family of Curves

Time (yrs)



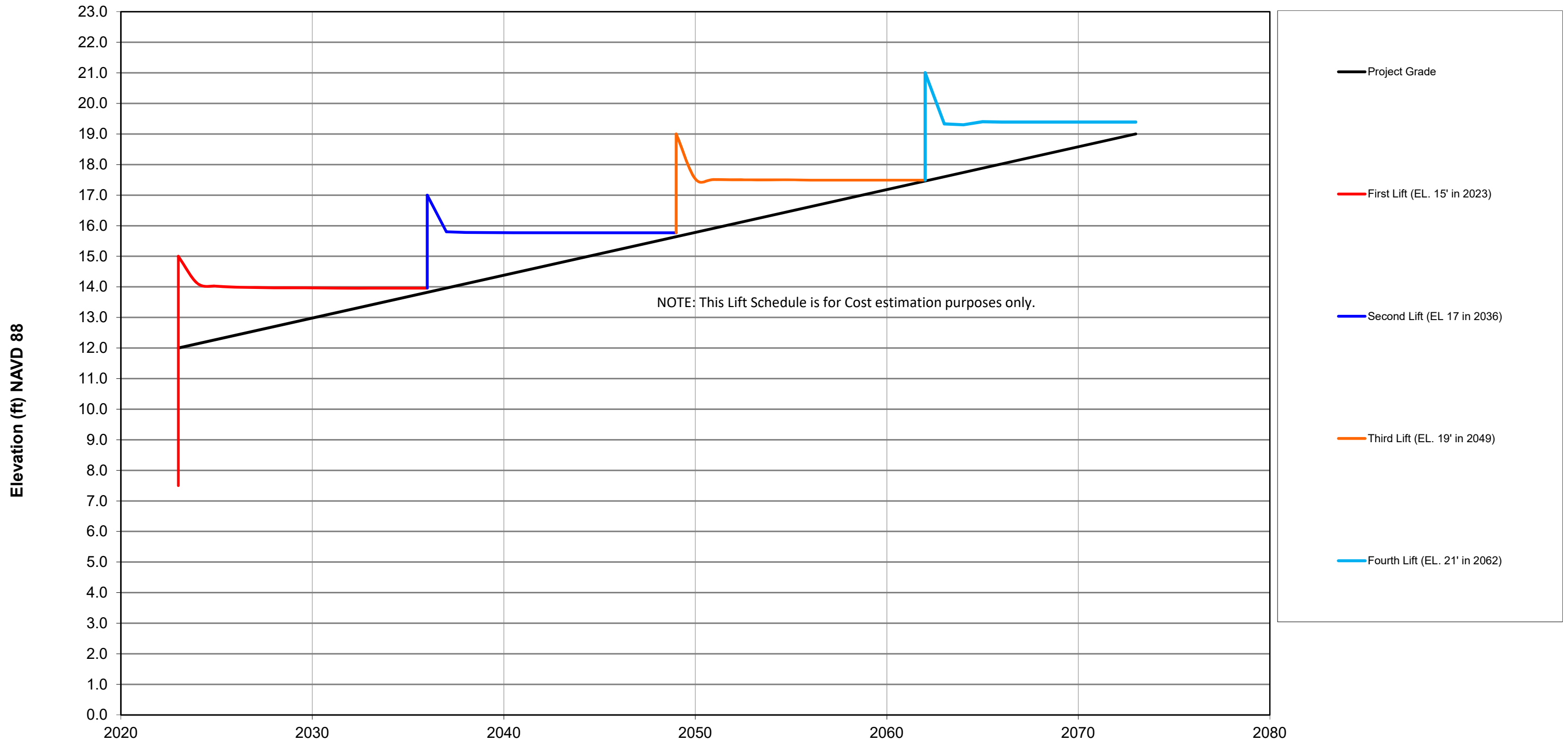
### Upper Barataria Basin Lift Schedule for Alternatives 1, 3 , and 5



NOTE: This Lift Schedule is for Cost estimation purposes only.

Note: Time-Rate Settlement Calculations are only an estimate. Time-Rate Settlement may vary from what is shown and is only developed for planning purposes.

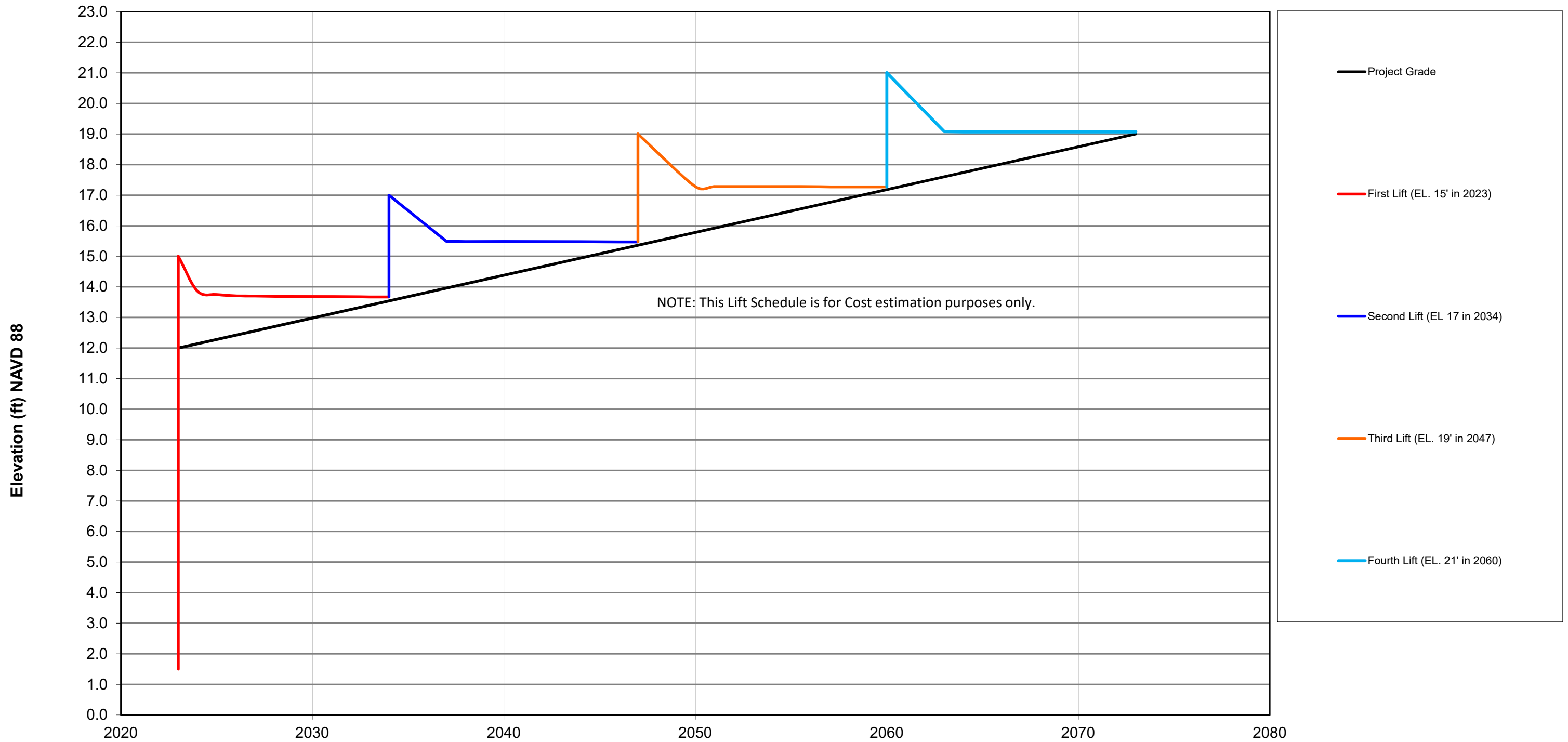
### Upper Barataria Basin Lift Schedule - Alternative 6 Reaches A, B and C



NOTE: This Lift Schedule is for Cost estimation purposes only.

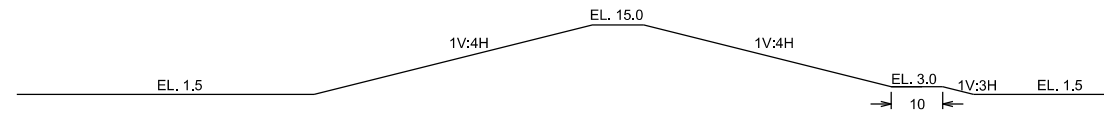
Note: Time-Rate Settlement Calculations are only an estimate. Time-Rate Settlement may vary from what is shown and is only developed for planning purposes.

### Upper Barataria Basin Lift Schedule - Alternative 6 - Reaches D, E, F, G, H and K

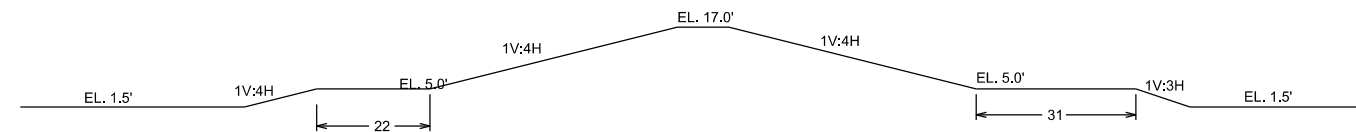


NOTE: This Lift Schedule is for Cost estimation purposes only.

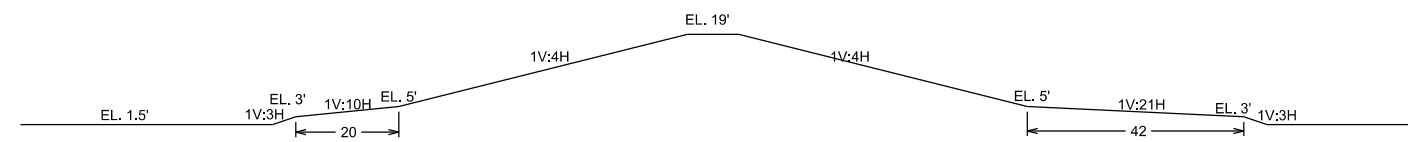
Note: Time-Rate Settlement Calculations are only an estimate. Time-Rate Settlement may vary from what is shown and is only developed for planning purposes.



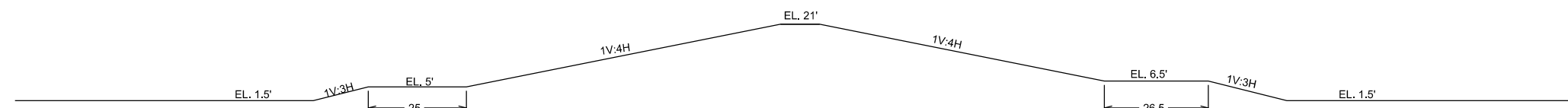
EL. 15' Upper Barataria Basin Section for Cost Estimation Purposes



EL. 17' Upper Barataria Basin Section for Cost Estimation Purposes



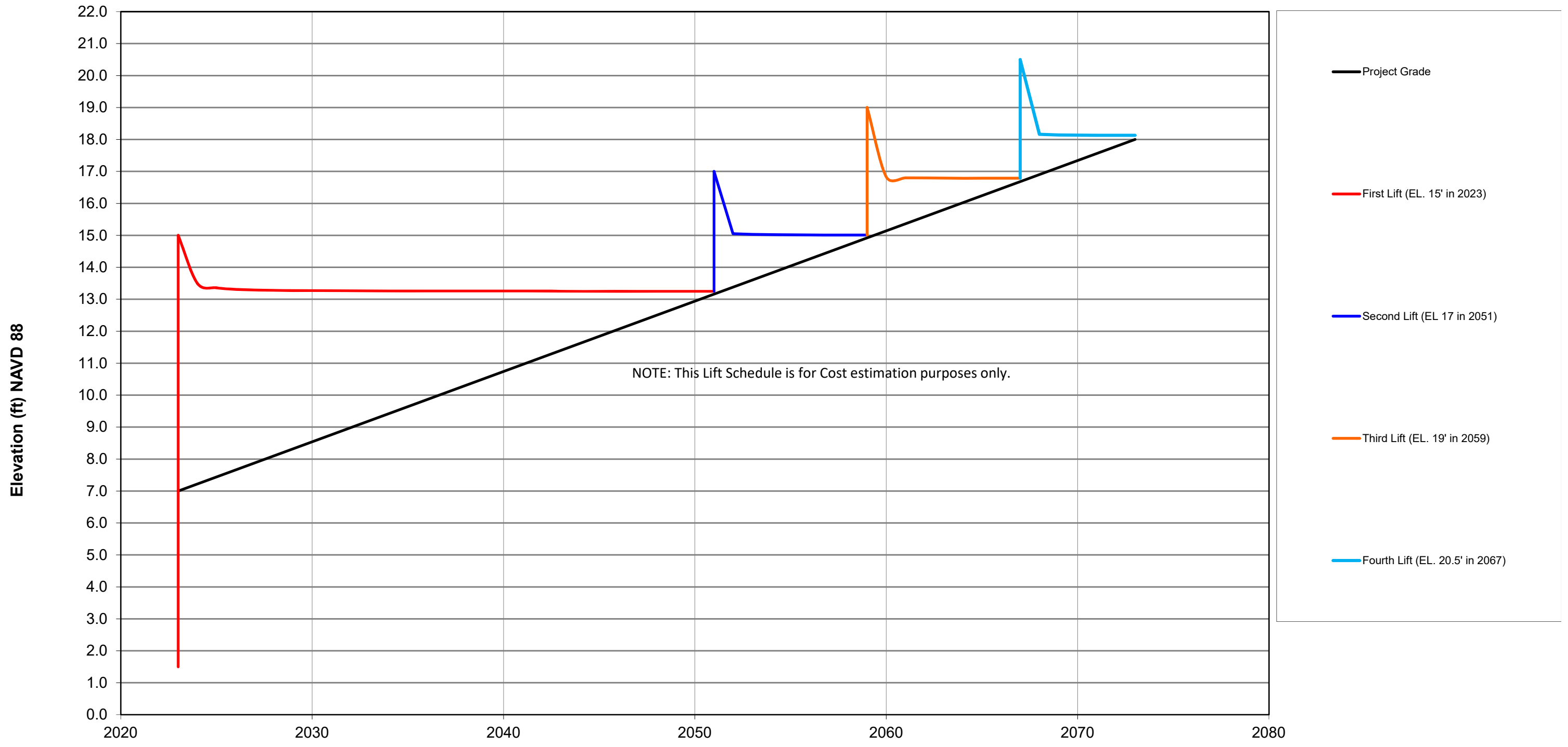
EL. 19' Upper Barataria Basin Section for Cost Estimation Purposes



EL. 21' Upper Barataria Basin Section for Cost Estimation Purposes

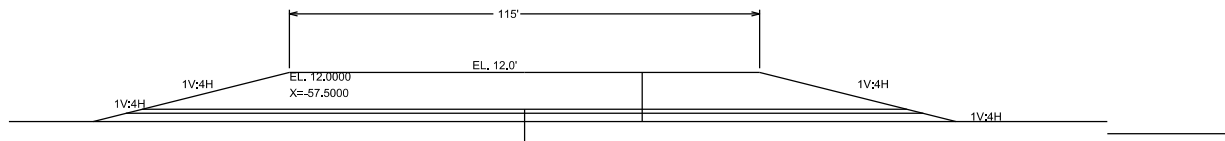
## Alternative 6 - Reaches A, B, C, D, E, F, G, H, and K

# Upper Barataria Basin Lift Schedule For Alternative 8 - Highway

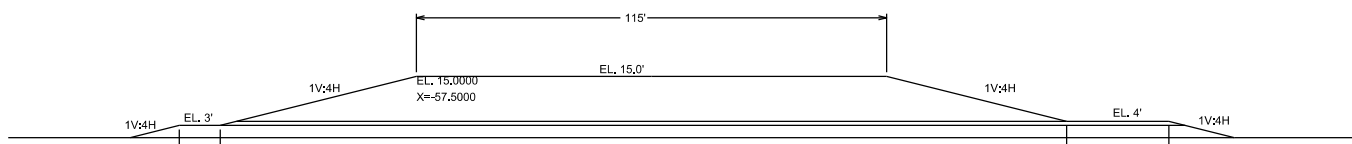


NOTE: This Lift Schedule is for Cost estimation purposes only.

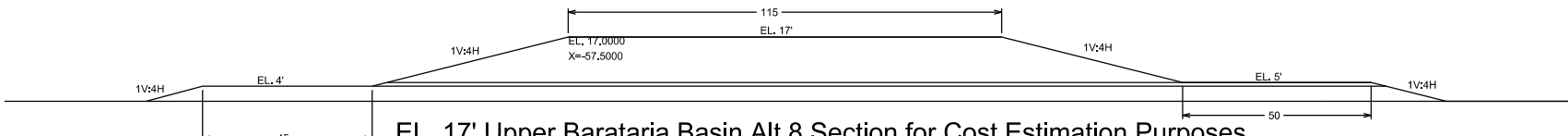
Note: Time-Rate Settlement Calculations are only an estimate. Time-Rate Settlement may vary from what is shown and is only developed for planning purposes.



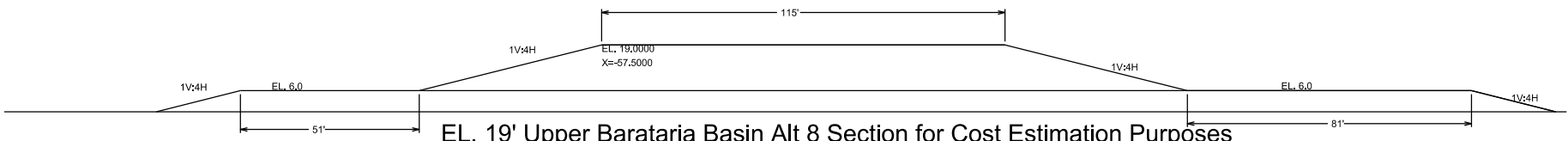
EL. 12' Upper Barataria Basin Alt 8 Section for Cost Estimation Purposes



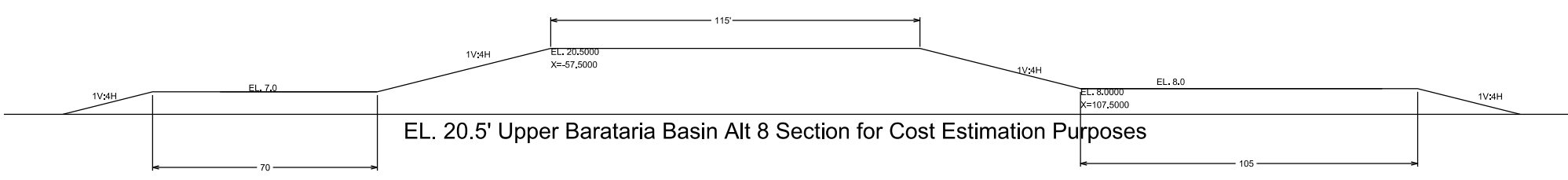
EL. 15' Upper Barataria Basin Alt 8 Section for Cost Estimation Purposes



EL. 17' Upper Barataria Basin Alt 8 Section for Cost Estimation Purposes



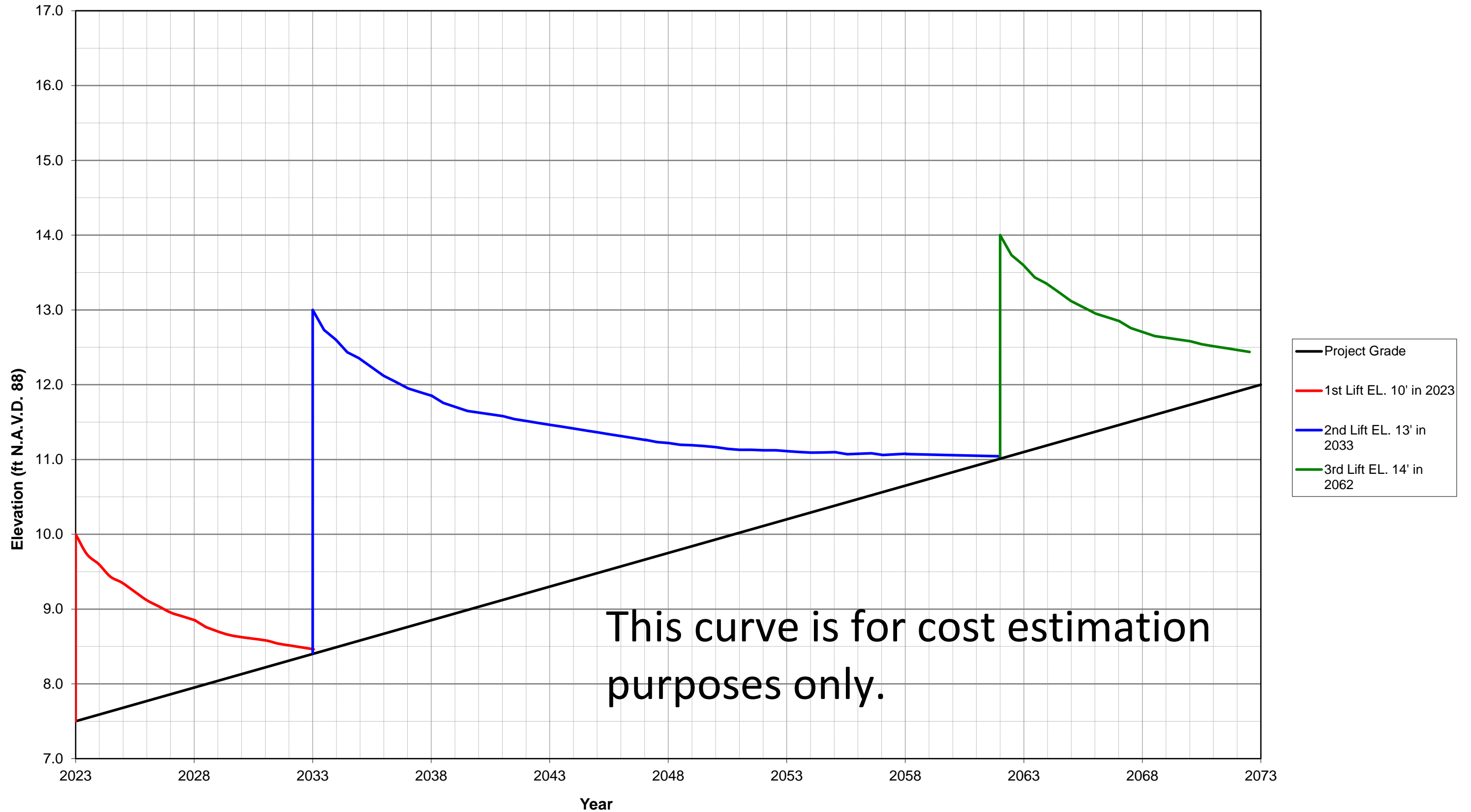
EL. 19' Upper Barataria Basin Alt 8 Section for Cost Estimation Purposes



EL. 20.5' Upper Barataria Basin Alt 8 Section for Cost Estimation Purposes

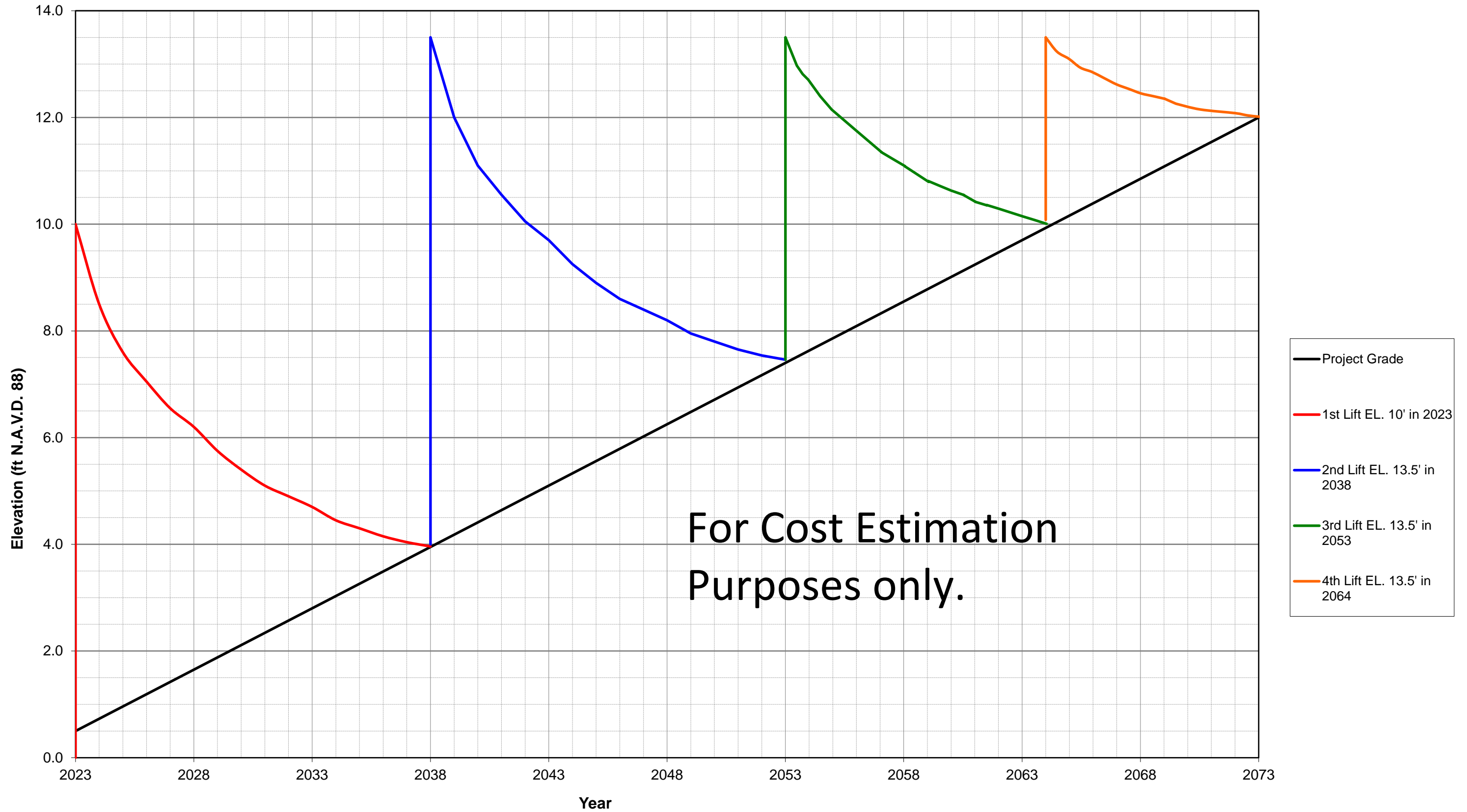
Alternative 8 - Reaches G, H, and I

Alternative 10  
Upper Barataria Basin Reaches A,B and C- Lift Schedule



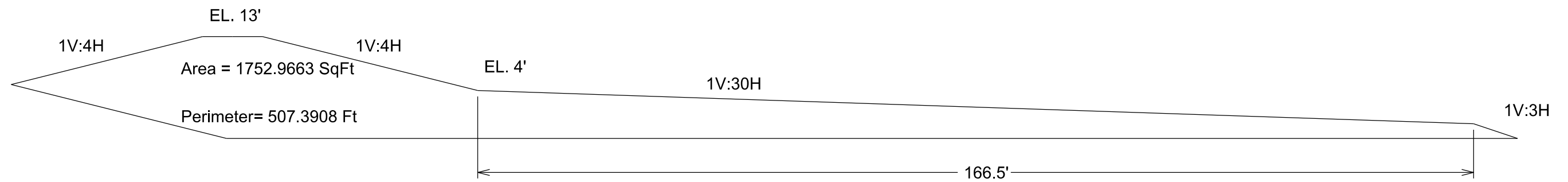


Upper Barataria Basin Reaches D to F - Lift Schedule



For Cost Estimation  
Purposes only.

# Typical Section used in the cost estimate to compare an alternative with a flood wall to a levee alternative



Typical Section from Appendix 8 of the Conceptual Design Report

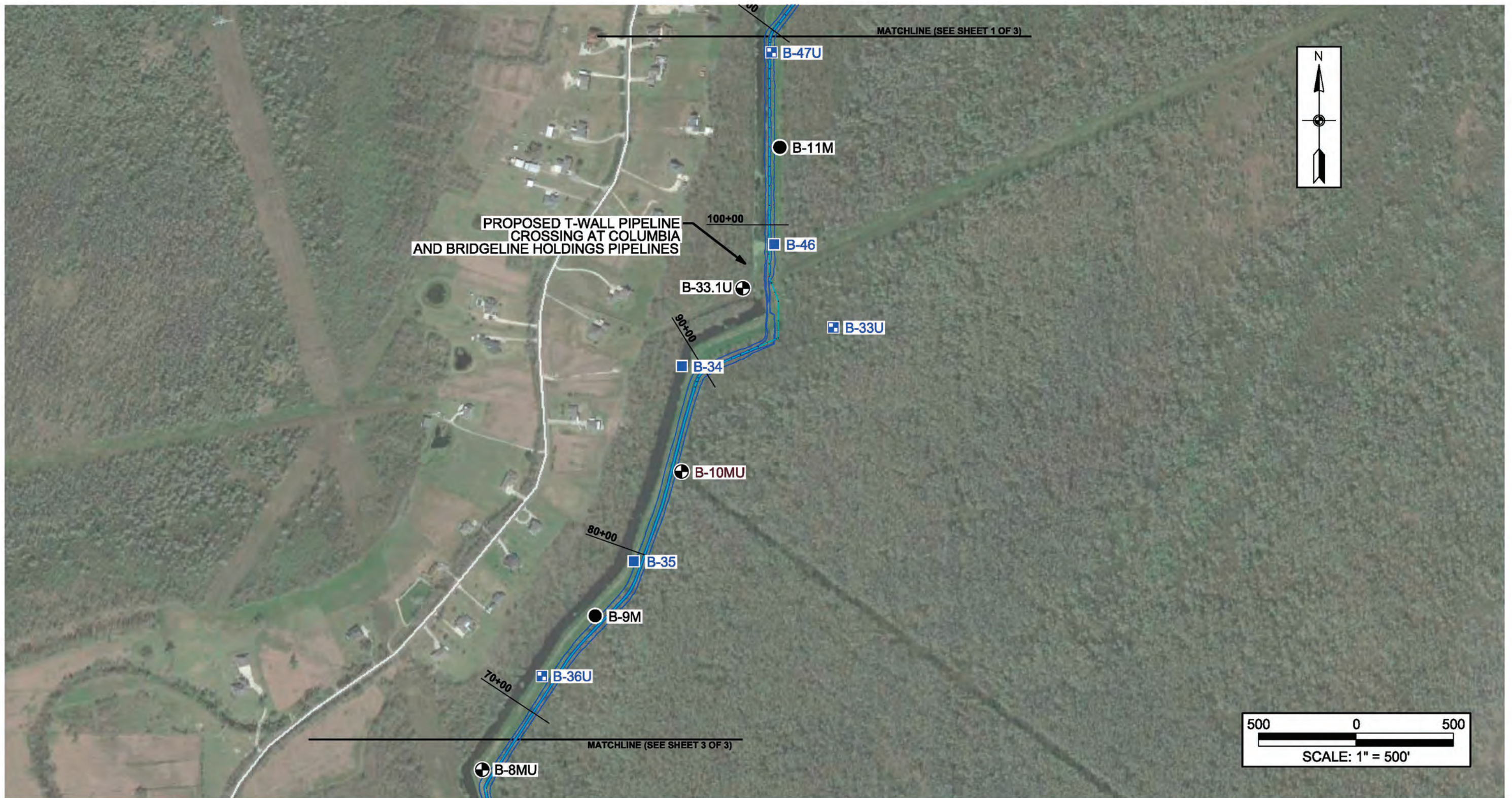
Upper Barataria Basin Risk Reduction  
CPRA Project 002HP.06 Segment 2 Typical Section Segment 2

Page 216 of 376 of the pdf. Sheet 13 of 71



- ⊕ DENOTES APPROXIMATE LOCATIONS OF 5-IN. UNDISTURBED SOIL BORINGS DRILLED BETWEEN APRIL 2014 AND JUNE 2015 FOR THIS PROJECT
- DENOTES APPROXIMATE LOCATIONS OF 3-IN. UNDISTURBED SOIL BORINGS DRILLED BETWEEN APRIL 2014 AND JUNE 2015 FOR THIS PROJECT
- ▣ DENOTES APPROXIMATE LOCATIONS OF 5-IN. UNDISTURBED SOIL BORINGS DRILLED IN 1995 AND 2004 UNDER EUSTIS ENGINEERING PROJECT NO. 13194
- DENOTES APPROXIMATE LOCATIONS OF 3-IN. UNDISTURBED SOIL BORINGS DRILLED IN 1995, 2003, AND 2004 UNDER EUSTIS ENGINEERING PROJECT NO. 13194

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<b>BORING LOCATION PLAN</b> ST. CHARLES PARISH MAGNOLIA RIDGE LEVEE PROJECT REPORT I - EARTHEN LEVEES ST. CHARLES PARISH, LOUISIANA ST. CHARLES PARISH PROJECT NO. P080905-6A		
DRAWN BY: J.L.S.	PLOT DATE: 12 NOV 15	CADD FILE: REPORT_I_PLAN.DGN
CHECKED BY: S.G.W.	JOB NO.: 22557	FIGURE 1 (SHEET 1 OF 3)



- ⊕ DENOTES APPROXIMATE LOCATIONS OF 5-IN. UNDISTURBED SOIL BORINGS DRILLED BETWEEN APRIL 2014 AND JUNE 2015 FOR THIS PROJECT
- DENOTES APPROXIMATE LOCATIONS OF 3-IN. UNDISTURBED SOIL BORINGS DRILLED BETWEEN APRIL 2014 AND JUNE 2015 FOR THIS PROJECT
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- DENOTES APPROXIMATE LOCATIONS OF 3-IN. UNDISTURBED SOIL BORINGS DRILLED IN 1995, 2003, AND 2004 UNDER EUSTIS ENGINEERING PROJECT NO. 13194

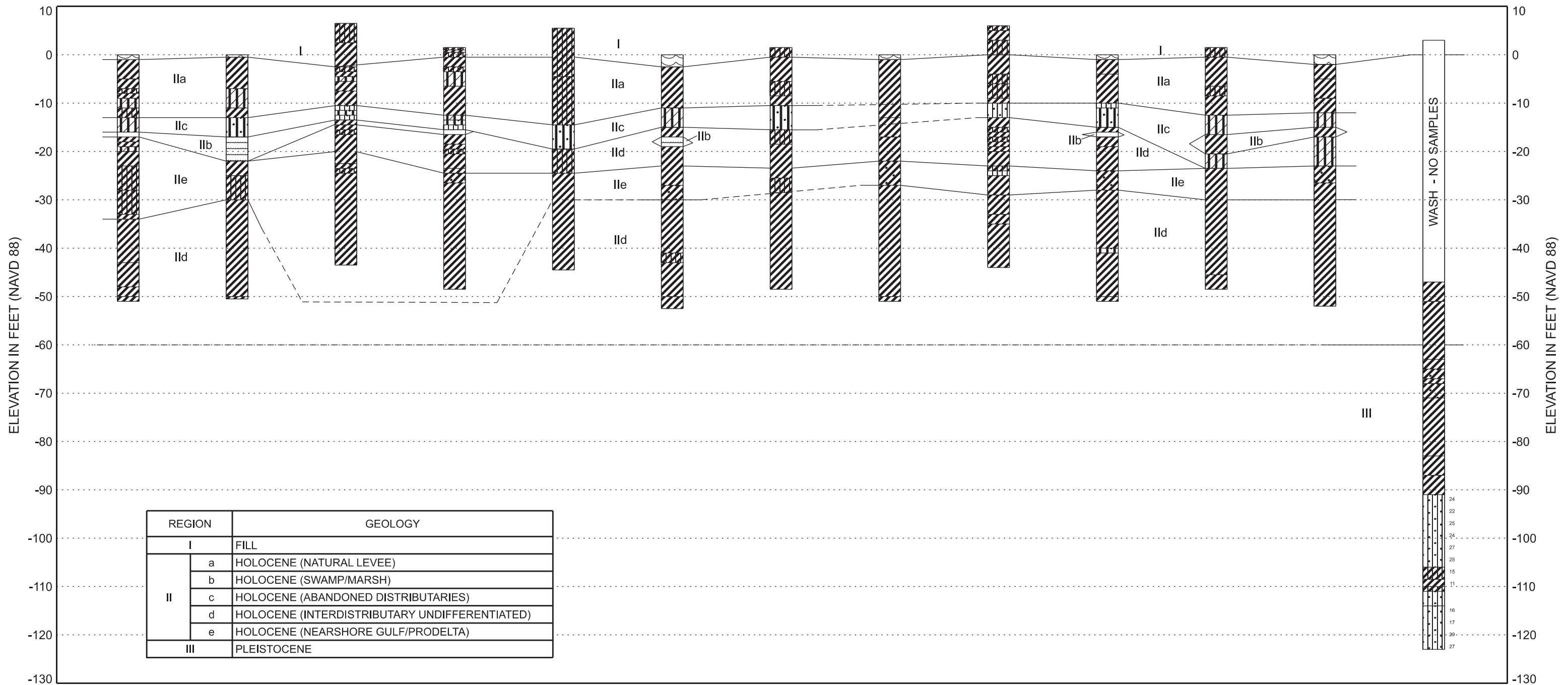
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DRAWN BY: J.L.S.	PLOT DATE: 12 NOV 15	CADD FILE: REPORT_I_PLAN.DGN
CHECKED BY: S.G.W.	JOB NO.: 22557	FIGURE 1 (SHEET 2 OF 3)



- ⊕ DENOTES APPROXIMATE LOCATIONS OF 5-IN. UNDISTURBED SOIL BORINGS DRILLED BETWEEN APRIL 2014 AND JUNE 2015 FOR THIS PROJECT
- DENOTES APPROXIMATE LOCATIONS OF 3-IN. UNDISTURBED SOIL BORINGS DRILLED BETWEEN APRIL 2014 AND JUNE 2015 FOR THIS PROJECT
- ⊕ DENOTES APPROXIMATE LOCATIONS OF 5-IN. UNDISTURBED SOIL BORINGS DRILLED IN 1995 AND 2004 UNDER EUSTIS ENGINEERING PROJECT NO. 13194
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<small>DRAWN BY: J.L.S.</small>	<small>PLOT DATE: 12 NOV 15</small>	<small>CADD FILE: REPORT_I_PLAN.DGN</small>
<small>CHECKED BY: S.G.W.</small>	<small>JOB NO.: 22557</small>	<small>FIGURE 1 (SHEET 3 OF 3)</small>

B-51 04 NOV 04 29°53'28.98" -90°23'9.96" G.S.E. 0.00	B-50 02 NOV 04 29°53'25.8" -90°23'17" G.S.E. 0.00	B-16MU 16 JUN 14 29°53'18.78" -90°23'22.26" G.S.E. 6.50	B-15MU 17 JUN 14 29°53'15.12" -90°23'25.92" G.S.E. 1.50	B-14M 18 JUN 14 29°33'28.8" -90°23'29.4" G.S.E. 5.50	B-49U 01 NOV 04 29°53'5.6" -90°23'30.4" G.S.E. 0.00	B-13M 19 JUN 14 29°53'4.02" -90°23'35.82" G.S.E. 1.50	B-48 29 OCT 04 29°52'59.6" -90°23'38.6" G.S.E. 0.00	B-12MU 25 JUN 14 29°52'56.58" -90°23'41.88" G.S.E. 6.00	B-47U 01 NOV 04 29°52'58.2" -90°23'43.9" G.S.E. 0.00	B-11M 26 JUN 14 29°52'47.28" -90°23'44.16" G.S.E. 1.50	B-46 01 NOV 04 29°52'42.2" -90°23'44.8" G.S.E. 0.00	B-33.1U 18 MAY 15 29°52'39" -90°23'44.4001" G.S.E. 3.00
--	---	---	---	--	---	---	---	---	--	--	---	---



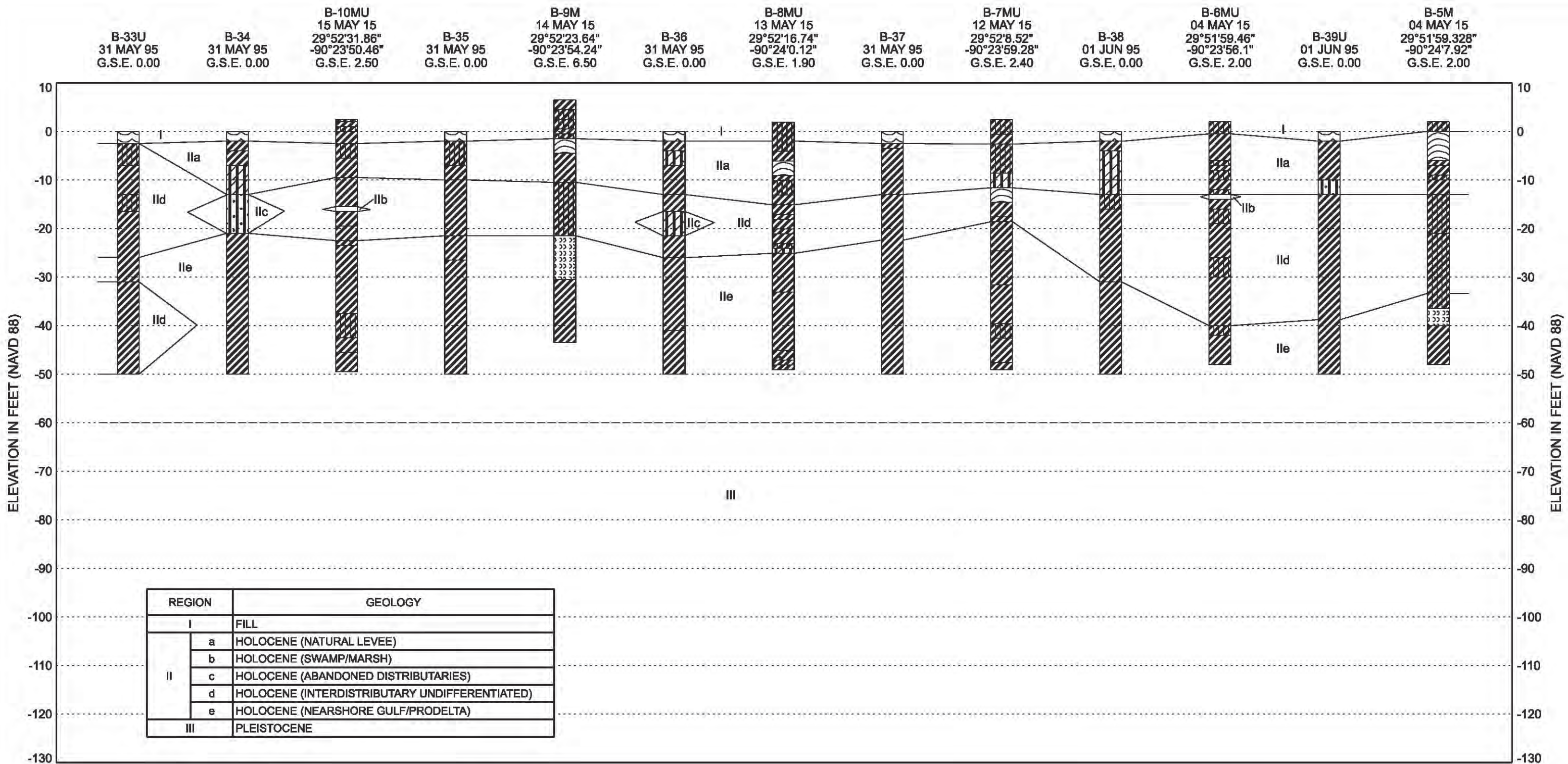
**BORING MATERIAL GRAPHICS**

- |             |              |       |
|-------------|--------------|-------|
| CLAY        | SANDY SILT   | WATER |
| SILTY CLAY  | CLAYEY SILT  |       |
| SANDY CLAY  | ORGANIC CLAY |       |
| SAND        | PEAT/HUMUS   |       |
| SILTY SAND  | WOOD         |       |
| CLAYEY SAND | SHELLS       |       |














**NOTE:**

NUMBERS TO THE RIGHT OF THE BORING LOGS ARE STANDARD PENETRATION TEST (SPT) RESULTS (I.E., "N-VALUES").

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DRAWN BY: J.L.S.	PLOT DATE: 12 NOV 15	CADD FILE: PROFILE.DGN
CHECKED BY: S.G.W.	JOB NO.: 22557	FIGURE 2 (SHEET 1 OF 3)




**BORING MATERIAL GRAPHICS**

-  CLAY
-  SILTY CLAY
-  SANDY CLAY
-  SAND
-  SILTY SAND
-  CLAYEY SAND
-  SANDY SILT
-  CLAYEY SILT
-  ORGANIC CLAY
-  PEAT/HUMUS
-  WOOD
-  SHELLS
-  WATER

**NOTE:**

NUMBERS TO THE RIGHT OF THE BORING LOGS ARE STANDARD PENETRATION TEST (SPT) RESULTS (I.E., "N-VALUES").



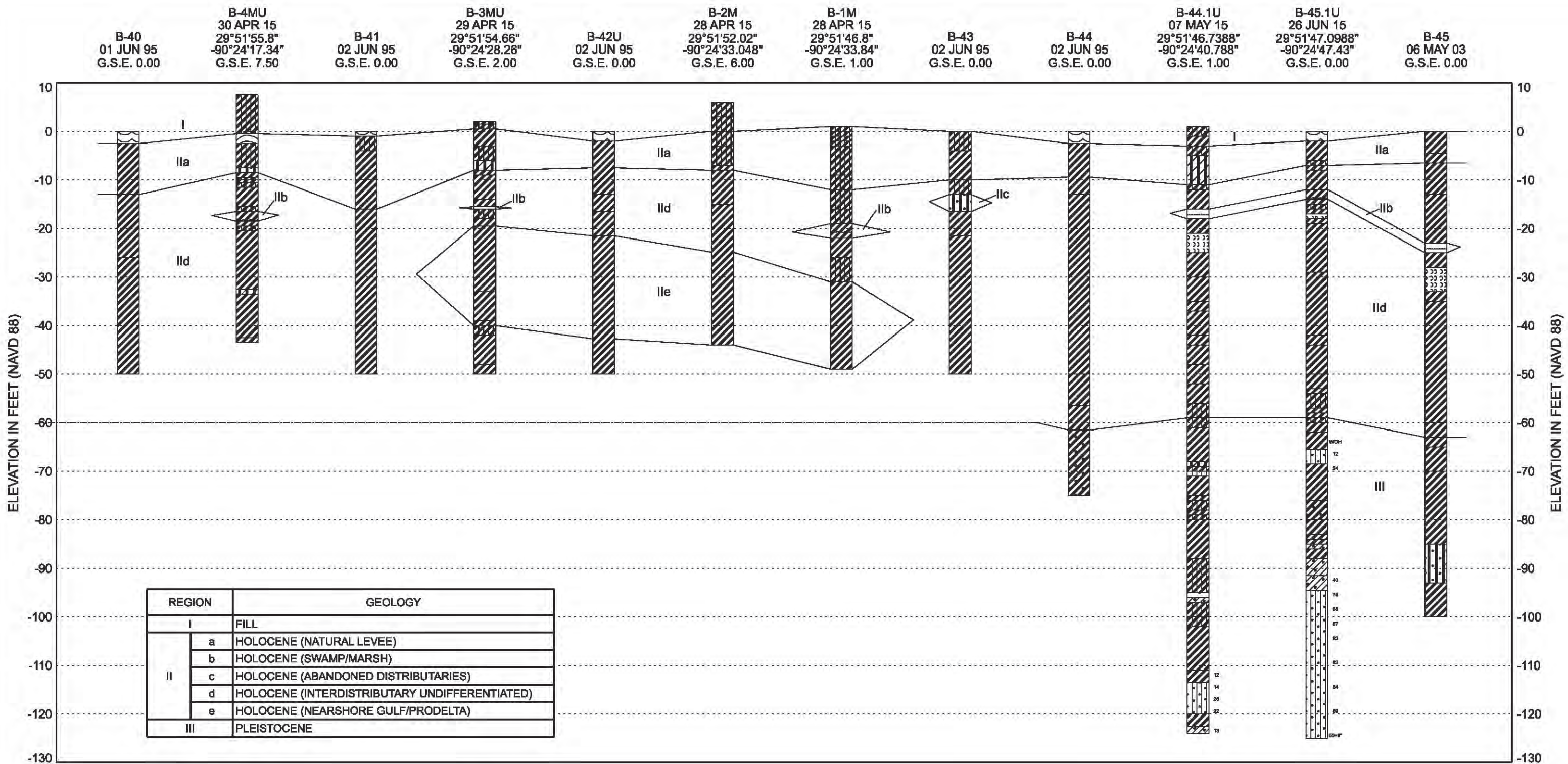
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---

**SUBSOIL PROFILE**

ST. CHARLES PARISH  
 MAGNOLIA RIDGE LEVEE PROJECT  
 REPORT I - EARTHEN LEVEES  
 ST. CHARLES PARISH, LOUISIANA  
 ST. CHARLES PARISH PROJECT NO. P080905-6A

DRAWN BY: J.L.S.	PLOT DATE: 12 NOV 15	CADD FILE: PROFILE.DGN
CHECKED BY: S.G.W.	JOB NO.: 22557	FIGURE 2 (SHEET 2 OF 3)



REGION	GEOLOGY
I	FILL
II	a HOLOCENE (NATURAL LEVEE)
	b HOLOCENE (SWAMP/MARSH)
	c HOLOCENE (ABANDONED DISTRIBUTARIES)
	d HOLOCENE (INTERDISTRIBUTARY UNDIFFERENTIATED)
	e HOLOCENE (NEARSHORE GULF/PRODELTA)
III	PLEISTOCENE

**BORING MATERIAL GRAPHICS**

- CLAY
- SILTY CLAY
- SANDY CLAY
- SAND
- SILTY SAND
- CLAYEY SAND
- SANDY SILT
- CLAYEY SILT
- ORGANIC CLAY
- PEAT/HUMUS
- WOOD
- SHELLS
- WATER

**NOTE:**

NUMBERS TO THE RIGHT OF THE BORING LOGS ARE STANDARD PENETRATION TEST (SPT) RESULTS (I.E., "N-VALUES").

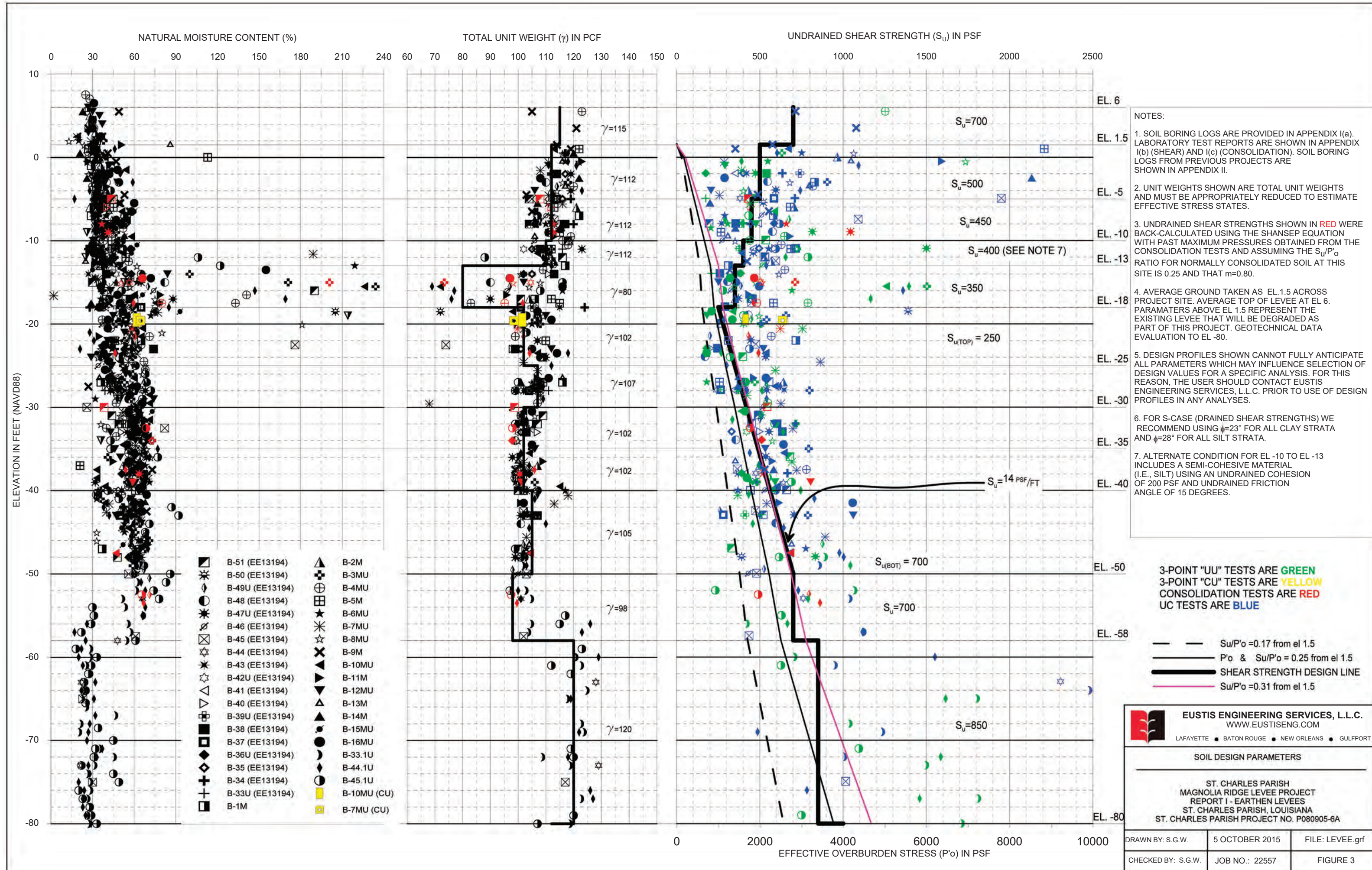
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**SUBSOIL PROFILE**

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 MAGNOLIA RIDGE LEVEE PROJECT  
 REPORT I - EARTHEN LEVEES  
 ST. CHARLES PARISH, LOUISIANA  
 ST. CHARLES PARISH PROJECT NO. P080905-6A**

DRAWN BY: J.L.S.	PLOT DATE: 12 NOV 15	CADD FILE: PROFILE.DGN
CHECKED BY: S.G.W.	JOB NO.: 22557	FIGURE 2 (SHEET 3 OF 3)





NOTES:

1. SOIL BORING LOGS ARE PROVIDED IN APPENDIX I(a). LABORATORY TEST REPORTS ARE SHOWN IN APPENDIX I(b) (SHEAR) AND I(c) (CONSOLIDATION). SOIL BORING LOGS FROM PREVIOUS PROJECTS ARE SHOWN IN APPENDIX II.
2. UNIT WEIGHTS SHOWN ARE TOTAL UNIT WEIGHTS AND MUST BE APPROPRIATELY REDUCED TO ESTIMATE EFFECTIVE STRESS STATES.
3. UNDRAINED SHEAR STRENGTHS SHOWN IN RED WERE BACK-CALCULATED USING THE SHANSEP EQUATION WITH PAST MAXIMUM PRESSURES OBTAINED FROM THE CONSOLIDATION TESTS AND ASSUMING THE  $S_u/P'_o$  RATIO FOR NORMALLY CONSOLIDATED SOIL AT THIS SITE IS 0.25 AND THAT  $m=0.80$ .
4. AVERAGE GROUND TAKEN AS EL. 1.5 ACROSS PROJECT SITE. AVERAGE TOP OF LEVEE AT EL. 6. PARAMETERS ABOVE EL. 1.5 REPRESENT THE EXISTING LEVEE THAT WILL BE DEGRADED AS PART OF THIS PROJECT. GEOTECHNICAL DATA EVALUATION TO EL. -80.
5. DESIGN PROFILES SHOWN CANNOT FULLY ANTICIPATE ALL PARAMETERS WHICH MAY INFLUENCE SELECTION OF DESIGN VALUES FOR A SPECIFIC ANALYSIS. FOR THIS REASON, THE USER SHOULD CONTACT EUSTIS ENGINEERING SERVICES, L.L.C. PRIOR TO USE OF DESIGN PROFILES IN ANY ANALYSES.
6. FOR S-CASE (DRAINED SHEAR STRENGTHS) WE RECOMMEND USING  $\phi=23^\circ$  FOR ALL CLAY STRATA AND  $\phi=28^\circ$  FOR ALL SILT STRATA.
7. ALTERNATE CONDITION FOR EL. -10 TO EL. -13 INCLUDES A SEMI-COHESIVE MATERIAL (I.E., SILT) USING AN UNDRAINED COHESION OF 200 PSF AND UNDRAINED FRICTION ANGLE OF 15 DEGREES.

3-POINT "UU" TESTS ARE GREEN  
 3-POINT "CU" TESTS ARE YELLOW  
 CONSOLIDATION TESTS ARE RED  
 UC TESTS ARE BLUE

---  $S_u/P'_o = 0.17$  from el. 1.5  
 ---  $P'_o$  &  $S_u/P'_o = 0.25$  from el. 1.5  
 ——— SHEAR STRENGTH DESIGN LINE  
 ———  $S_u/P'_o = 0.31$  from el. 1.5

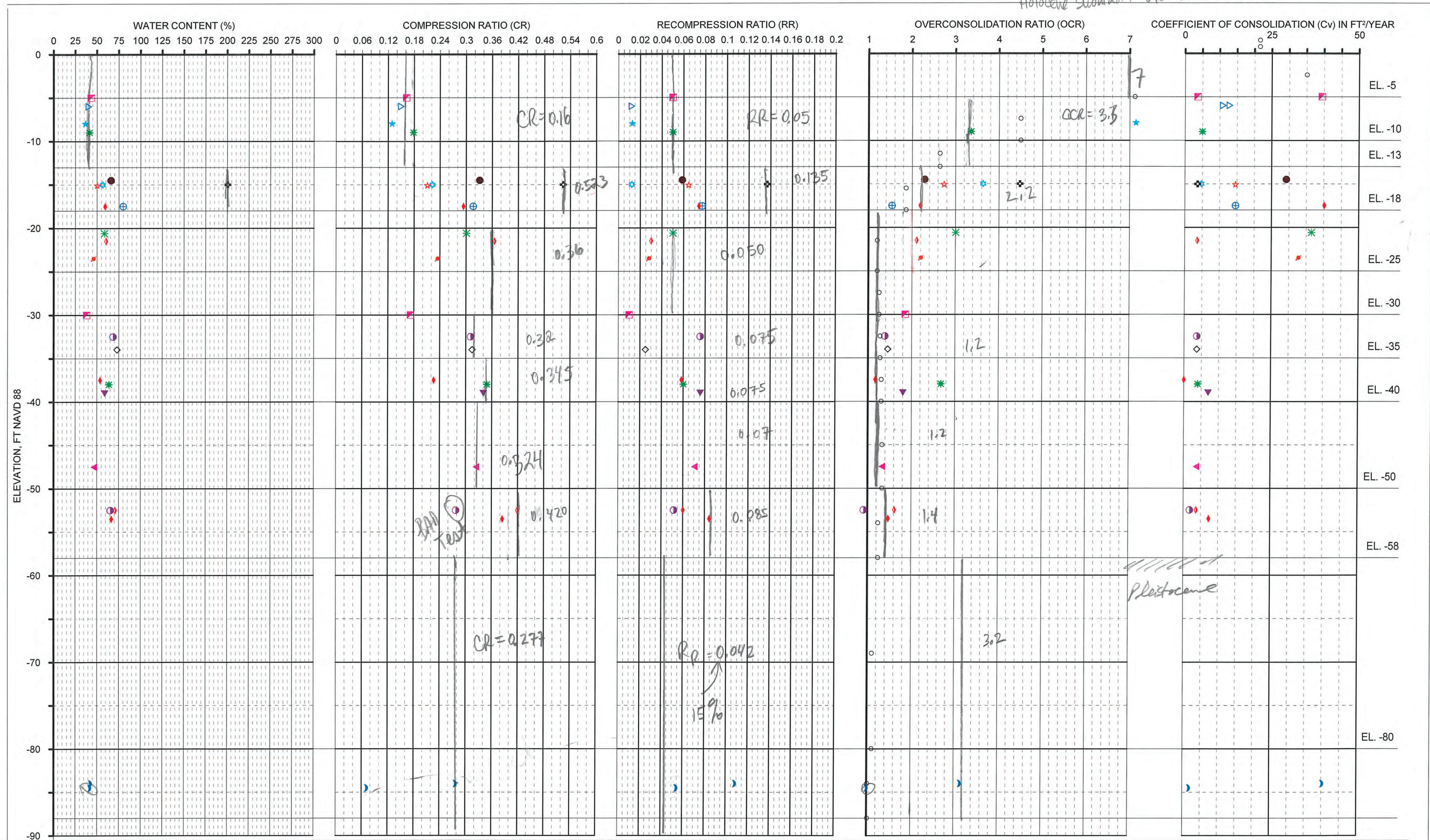
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SOIL DESIGN PARAMETERS

ST. CHARLES PARISH  
 MAGNOLIA RIDGE LEVEE PROJECT  
 REPORT I - EARTHEN LEVEES  
 ST. CHARLES PARISH, LOUISIANA  
 ST. CHARLES PARISH PROJECT NO. P080905-6A

DRAWN BY: S.G.W.	5 OCTOBER 2015	FILE: LEVEE.grf
CHECKED BY: S.G.W.	JOB NO.: 22557	FIGURE 3

*Holocene shouldn't use ocr > 1.1 (???)*



- |   |           |   |             |   |             |   |              |   |              |   |                   |   |                     |   |                     |   |                    |   |                       |
|---|-----------|---|-------------|---|-------------|---|--------------|---|--------------|---|-------------------|---|---------------------|---|---------------------|---|--------------------|---|-----------------------|
| + | B-3MU, 6B | * | B-7MU, 8C   | ▽ | B-12MU, 13B | ◐ | B-33.1U, 10B | ◇ | B-44.1U, 11C | ○ | B-45.1U, 13C      | ☆ | B-44, 5 (EE13194)   | * | B-47, 3B (EE13194)  | ◇ | B-49, 5C (EE13194) | ◻ | B-51, 8C (EE13194)    |
| ⊕ | B-4MU, 9B | ☆ | B-8MU, 6C   | ◐ | B-15MU, 8B  | ◑ | B-33.1U, 10B | ◇ | B-44.1U, 15C | ○ | B-35, 9 (EE13194) | * | B-47, 10C (EE13194) | * | B-49, 13C (EE13194) | ◻ | B-51, 2B (EE13194) | ○ | SHANSEP_OCR           |
| ★ | B-6MU, 4C | ◀ | B-10MU, 14C | ● | B-16MU, 7B  | ◑ | B-44.1U, 6C  | ◐ | B-45.1U, 8C  | ◑ | B-40, 2 (EE13194) | * |                     | * |                     |   |                    |   | $m=0.8$<br>$c_s=0.25$ |

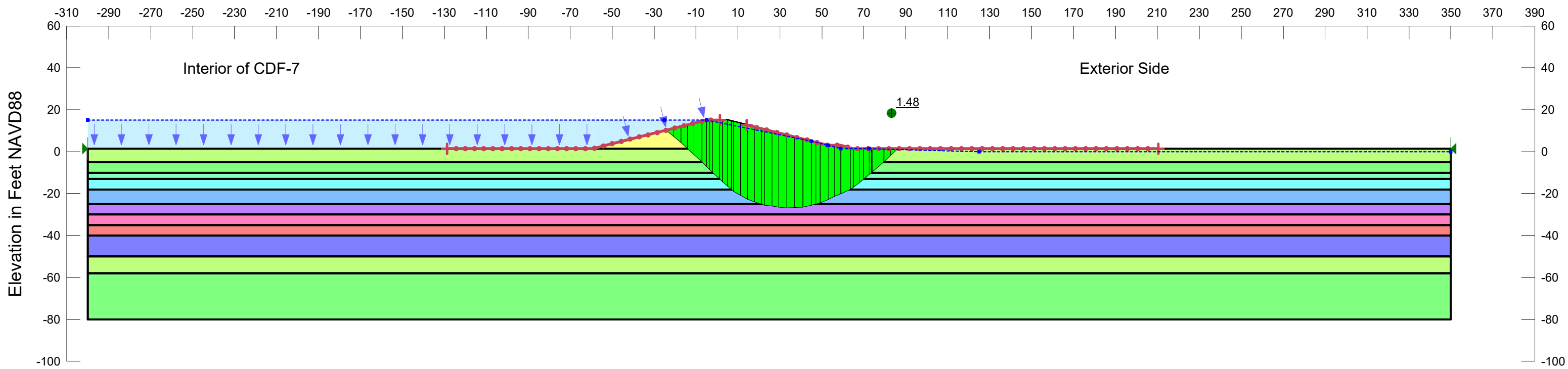
EE 22557  
Magnolia Ridge  
Consolidation Test Summary

Homogeneous CL and CH sedimentary clays of low to moderate sensitivity ( $I_p = 20\% - 80\%$ ):  
 $S = 0.20 + 0.05I_p$ , or simply  $S = 0.22$ .  
 $m = 0.88(1 - C_c/C_u) \pm 0.06 SD$ , or simply  $m = 0.8$ .  
 Sedimentary deposits of silts and organic soils (Atterberg limits plot below the A-line, but excluding peats) and clays with shells:  
 $S = 0.25$ , with nominal  $SD = 0.05$ .  
 $m = 0.88(1 - C_c/C_u) \pm 0.06 SD$ , or simply  $m = 0.8$ .

$$\frac{C_u}{\sigma'_{vc}} = S(OCR)^m$$

0.8 = m  
0.25 = S

No.	Boring	Sample	Boring El. (feet)	Sample Depth (feet)	Sample El. (feet)	USCS	w%	Cc	Cs	eo	CR	RR Based on Consol Test	Theoretical RR=.15*CR	Dry Unit Weight (pcf)	Moist Unit Weight (pcf)	Approximate P'o (Psf)	Approximate P'o (tsf)	Approximate P'c (tsf)	OCR = P'o/P'o	S <sub>v</sub> = P'o*S*(P' <sub>v</sub> /C <sub>u</sub> ) <sup>m</sup>	C <sub>v</sub> (sq.ft/year)	Remarks	
1	B12MU	13B	6.0	45.0	-39.0	CH	59.1	0.911	0.202	1.674	0.341	0.076	0.051	63.6	101.2	2005.0	1.00	1.81	1.81	804	45	7.00	591
2	B15MU	8B	1.5	25.0	-23.5	CH	46.3	0.628	0.075	1.674	0.235	0.028	0.035	71.2	104.2	1042.0	0.52	1.15	2.21	491	60	32.85	268
3	B16MU	7B	6.5	21.0	-14.5	CH	66.0	0.968	0.171	1.925	0.331	0.059	0.050	58.5	97.1	960.6	0.48	1.10	2.29	466	73	29.20	320
4	B3MU	6B	2.0	17.0	-15.0	OH	200.8	3.279	0.858	5.268	0.523	0.137	0.078	24.4	73.4	856.2	0.43	1.92	4.48	711	18	3.65	1503
5	B4MU	9B	7.5	25.0	-17.5	OH	79.9	0.989	0.240	2.126	0.316	0.077	0.047	52.9	95.2	1363.0	0.68	1.05	1.54	482	29	14.60	788
6	B6MU	4C	2.0	10.0	-8.0	CL	36.7	0.264	0.026	1.044	0.129	0.012	0.019	82.5	112.8	546.0	0.27	1.95	7.14	658	365	365.00	306/205
7	B7MU	8C	2.4	23.0	-20.6	CH	58.6	0.807	0.134	1.680	0.301	0.050	0.045	62.9	99.8	1030.0	0.52	1.55	3.01	622	219	36.50	CU=381; UU=755
8	B8MU	6C	1.9	17.0	-15.1	CH	50.4	0.549	0.168	1.602	0.211	0.064	0.032	65.3	98.2	912.2	0.46	1.25	2.74	511	29	14.60	475
9	B10MU	14C	2.5	50.0	-47.5	CH	46.9	0.779	0.170	1.405	0.324	0.071	0.049	71.1	104.4	2181.0	1.09	1.45	1.33	685	32	3.65	679
10	B33.1U	10B 3' test	3.0	87.0	-84.0	CH	42.4	0.598	0.234	1.159	0.277	0.108	0.042	78.7	112.1	4205.2	2.10	6.60	3.14	2625		40.15	uu=1561/1846(Uc)
11	B33.1U	* 10B BAD TEST	3.0	87.5	-84.5	CH	41.7	0.153	0.116	1.142	0.071	0.054	0.011	79.3	112.4	4205.2	2.10	2.08	0.99	1042	29	1.83	uu=1561; 1846=Uc
12	B44.1U	6C	1.0	18.5	-17.5	OH	59.6	0.749	0.189	1.548	0.294	0.074	0.044	63.7	101.7	985.6	0.49	1.08	2.19	462	40	40.15	1165
13	B44.1U	11C	1.0	38.5	-37.5	CH	53.9	0.558	0.144	1.466	0.226	0.058	0.034	68.8	105.9	1881.0	0.94	1.10	1.17	533	29	0.00	492
14	B44.1U	15C	1.0	54.5	-53.5	CH	66.8	1.103	0.242	1.866	0.385	0.084	0.058	59.7	99.6	2526.5	1.26	1.86	1.47	861	22	3.65	1460
15	B45.1U	8C	0.0	32.5	-32.5	CH	68.6	0.908	0.220	1.922	0.311	0.075	0.047	58.1	98.0	1356.0	0.68	0.94	1.39	440	40	3.65	588
16	B45.1U	* 13C	0.0	52.5	-52.5	CH	65.5	0.806	0.149	1.904	0.278	0.051	0.042	58.9	97.5	2108.0	1.05	0.96	0.91	489	N/A	1.83	232
24	B35	9	0.0	34.0	-34.0	CH	73.0	0.950		2.023	0.314	0.025	0.047	56.6	97.9	1513.0	0.76	1.10	1.45	510	7.3	3.65	
25	B40	2	0.0	6.0	-6.0	CH	40.6	0.320		1.134	0.150	0.012	0.022	79.6	111.9	301.0	0.15	1.40	9.30	448	18	10.95	
26	B44	5	0.0	15.0	-15.0	CH	56.5	0.570		1.562	0.222	0.012	0.033	66.8	104.5	715.0	0.36	1.30	3.64	502	9	4.75	
27	B47	3B	0.0	9.0	-9.0	CH	41.4	0.380		1.130	0.178	0.050	0.027	79.7	112.7	441.0	0.79	2.66	3.35	1044	26	5.00	
28	B47	10C	0.0	38.0	-38.0	CH	63.7	0.970		1.781	0.349	0.060	0.052	61.5	100.7	1587.0	0.47	1.27	2.68	521	7	4.00	
29	B49	5C	0.0	21.5	-21.5	CH	60.7	0.980		1.679	0.366	0.030	0.055	63.4	101.9	948.0	0.47	1.00	2.11	431	22	3.65	
30	B49	13C	0.0	52.5	-52.5	CH	71.1	1.250		1.980	0.419	0.060	0.063	57.4	98.2	2166.5	1.08	1.75	1.62	795	48	3.65	
31	B51	2B	0.0	5.0	-5.0	CH	43.5	0.370		1.276	0.163	0.050	0.024	75.2	107.9	245.0	0.12	1.40	11.43	430	44	3.65	
32	B51	8C	0.0	30.0	-30.0	CL	38.4	0.360		1.084	0.173	0.010	0.026	71.3	98.7	1325.0	0.66	1.23	1.86	543	923	146.00	



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 22557-SCP-Magnolia Ridge Levee Project - Report I - Earthen Levees - Report and Figures. pdf  
 Page 45/49

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GENERAL NOTES

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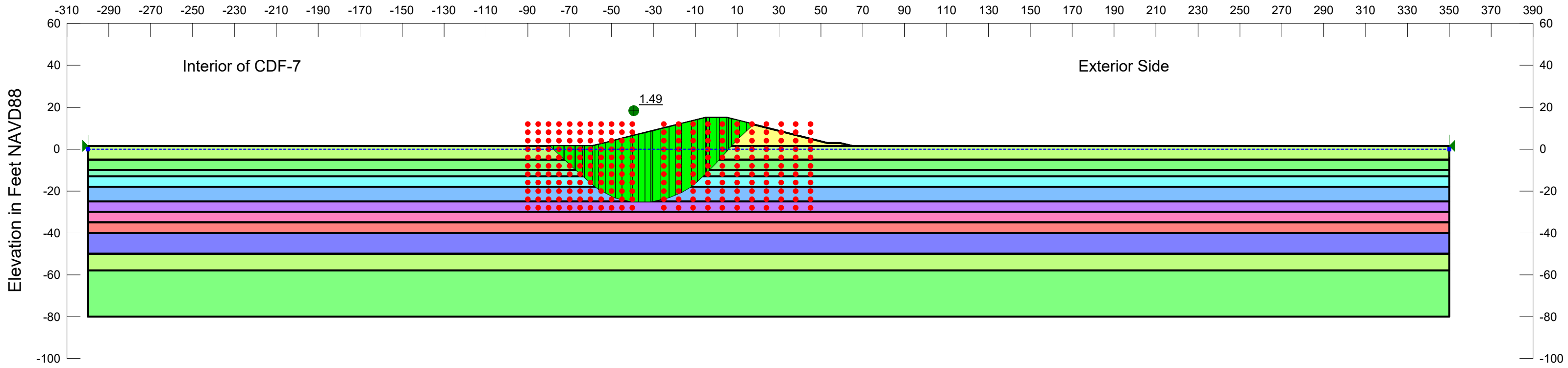
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**US Army Corps  
 of Engineers**  
 New Orleans District  
 Upper Barataria Basin  
 Stability Analysis for Cost Estimate  
 Alternative 6

Construction Grade - Entry Exit Slip Surface  
 Louisiana



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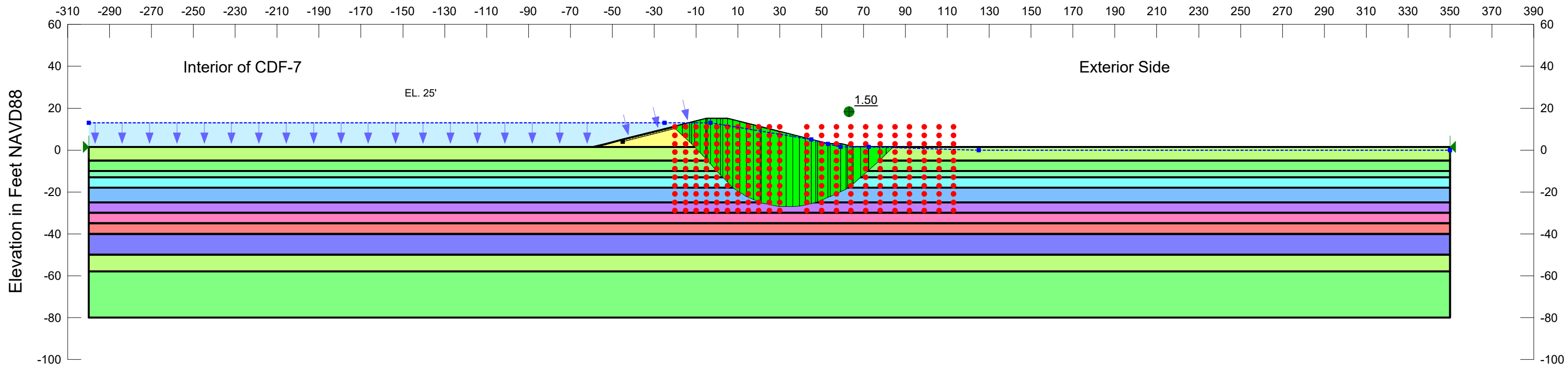
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**US Army Corps  
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 New Orleans District  
 Upper Barataria Basin  
 Stability Analysis for Cost Estimate  
 Alternative 6

Low Water Level - Block Slip Surface  
 Louisiana



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 Page 45/49

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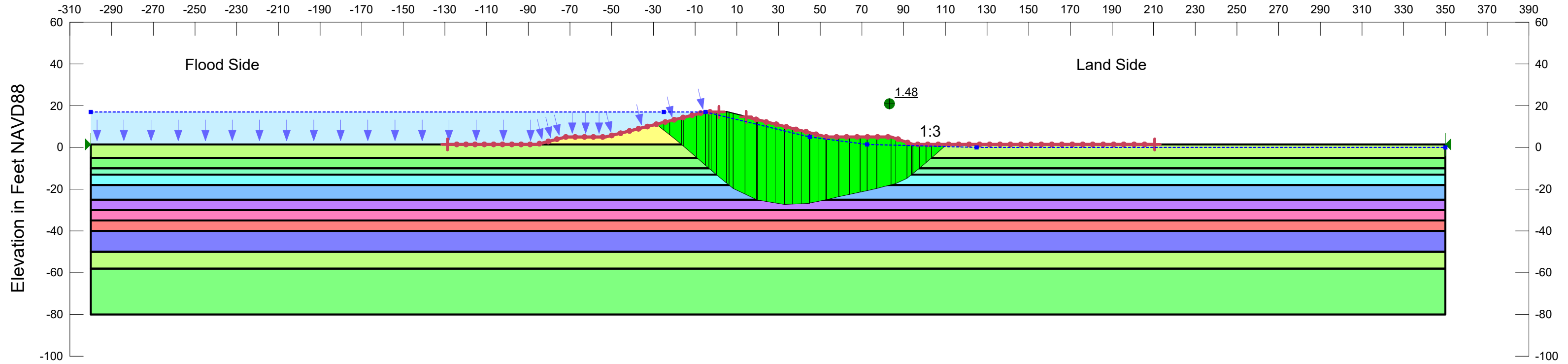
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**US Army Corps  
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 New Orleans District  
 Upper Barataria Basin  
 Stability Analysis for Cost Estimate  
 Alternative 6

Still Water Level - Block Slip Surface  
 Louisiana



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 22557-SCP-Magnolia Ridge Levee Project - Report I - Earthen Levees - Report and Figures. pdf  
 Page 45/49

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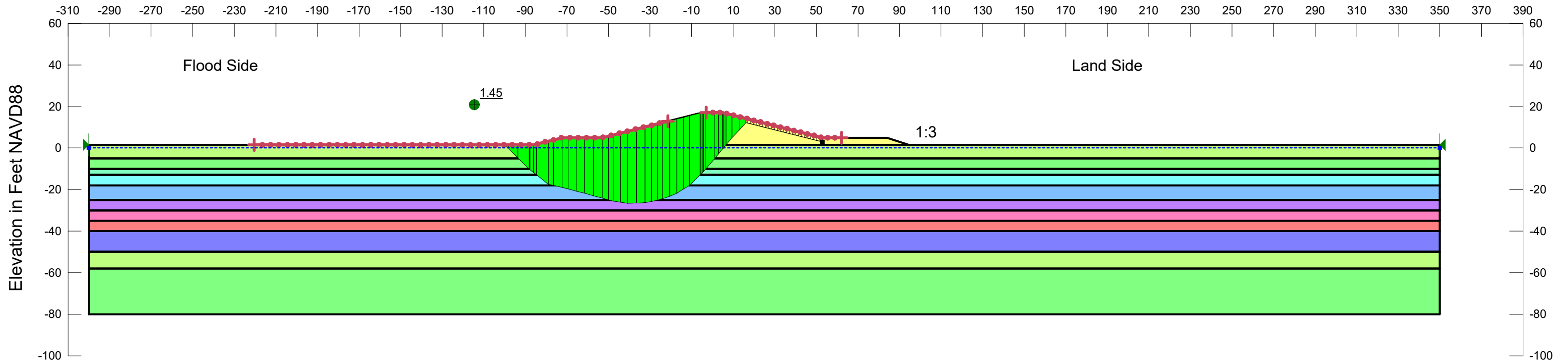
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**US Army Corps  
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 New Orleans District  
 Upper Barataria Basin  
 Stability Analysis for Cost Estimate  
 Alternative 6

Top of Levee - Entry Exit Slip Surface  
 Louisiana



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 22557-SCP-Magnolia Ridge Levee Project - Report I - Earthen Levees - Report and Figures. pdf  
 Page 45/49

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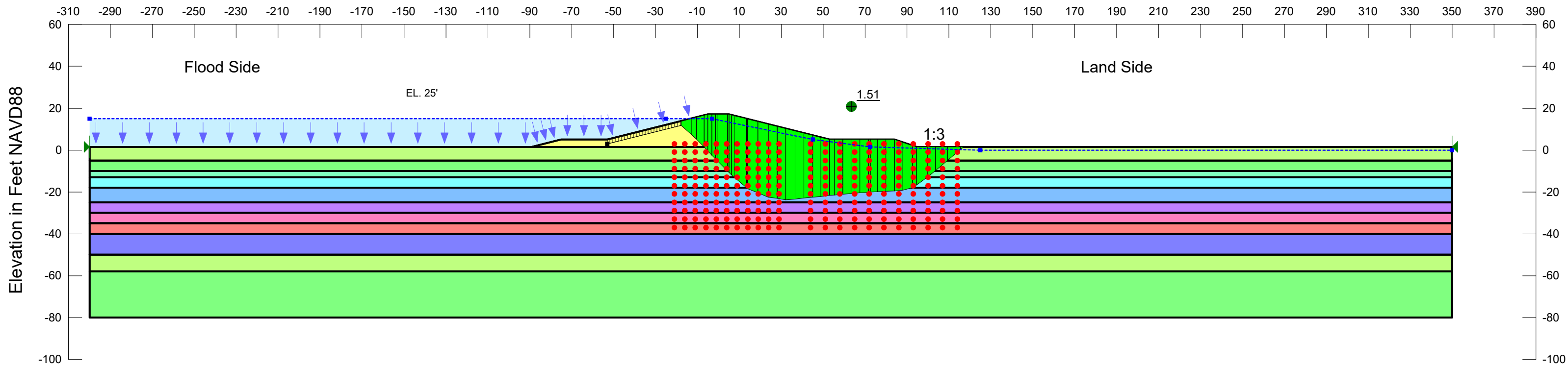
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**US Army Corps  
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 New Orleans District  
 Upper Barataria Basin  
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 Alternative 6

Low Water Level - Entry Exit Slip Surface  
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 22557-SCP-Magnolia Ridge Levee Project - Report I - Earthen Levees - Report and Figures. pdf  
 Page 45/49

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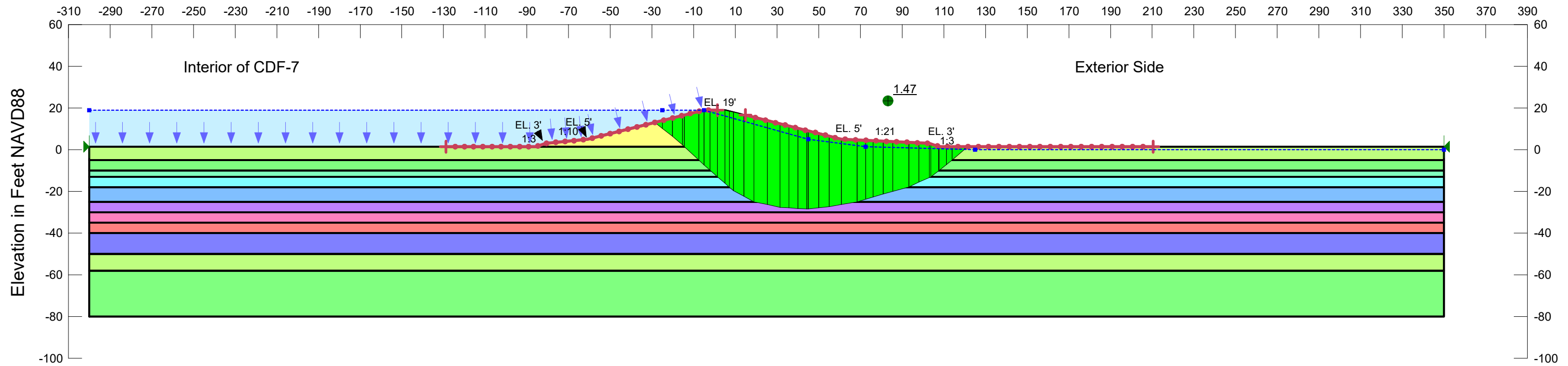
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**US Army Corps  
 of Engineers**  
 New Orleans District  
 Upper Barataria Basin  
 Stability Analysis for Cost Estimate  
 Alternative 6

Still Water Level - Block Slip Surface  
 Louisiana



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 22557-SCP-Magnolia Ridge Levee Project - Report I - Earthen Levees - Report and Figures. pdf  
 Page 45/49

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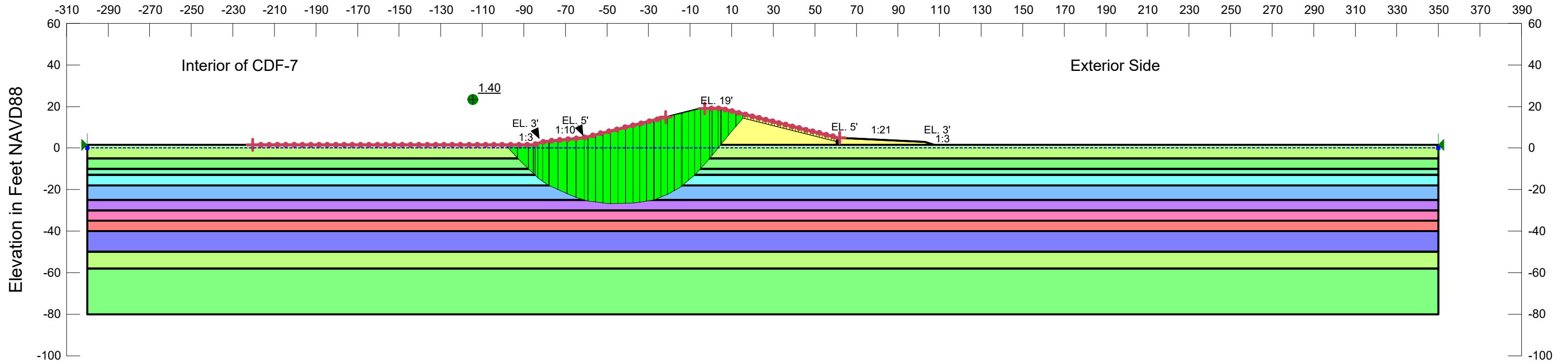
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**US Army Corps  
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 New Orleans District  
 Upper Barataria Basin  
 Stability Analysis for Cost Estimate  
 Alternative 6

Top of Levee - Entry Exit Slip Surface  
 Louisiana



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 Page 45/49

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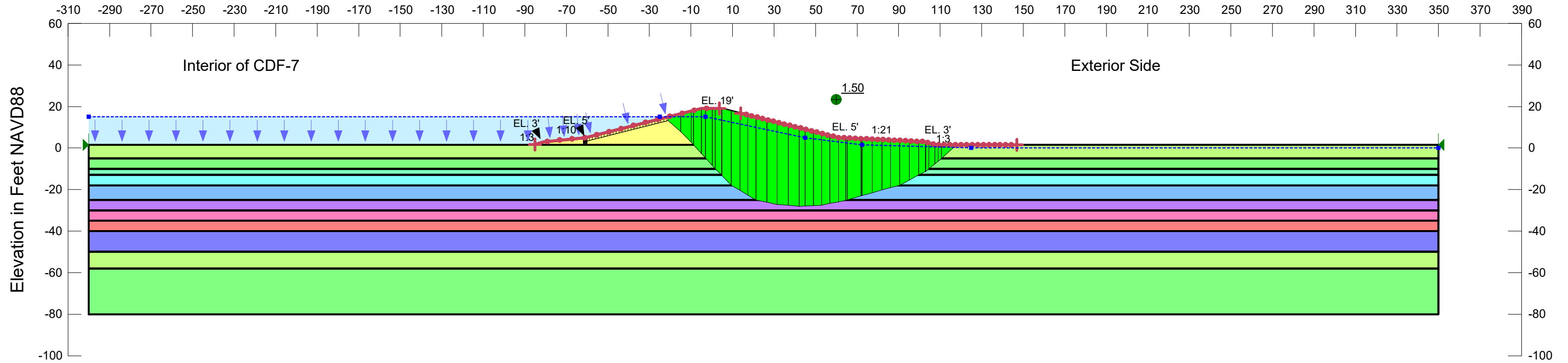
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**US Army Corps  
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 New Orleans District  
 Upper Barataria Basin  
 Stability Analysis for Cost Estimate  
 Alternative 6

Low Water Level - Entry Exit Slip Surface  
 Louisiana



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 22557-SCP-Magnolia Ridge Levee Project - Report I - Earthen Levees - Report and Figures. pdf  
 Page 45/49

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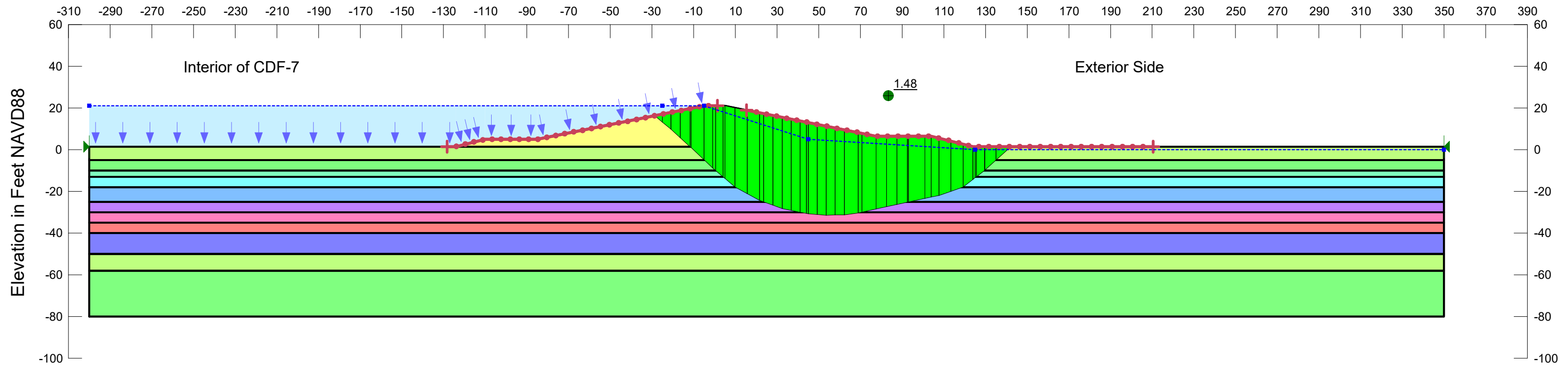
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**US Army Corps  
 of Engineers**  
 New Orleans District  
 Upper Barataria Basin  
 Stability Analysis for Cost Estimate  
 Alternative 6

Still Water Level - Entry Exit Slip Surface  
 Louisiana



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 22557-SCP-Magnolia Ridge Levee Project - Report I - Earthen Levees - Report and Figures. pdf  
 Page 45/49

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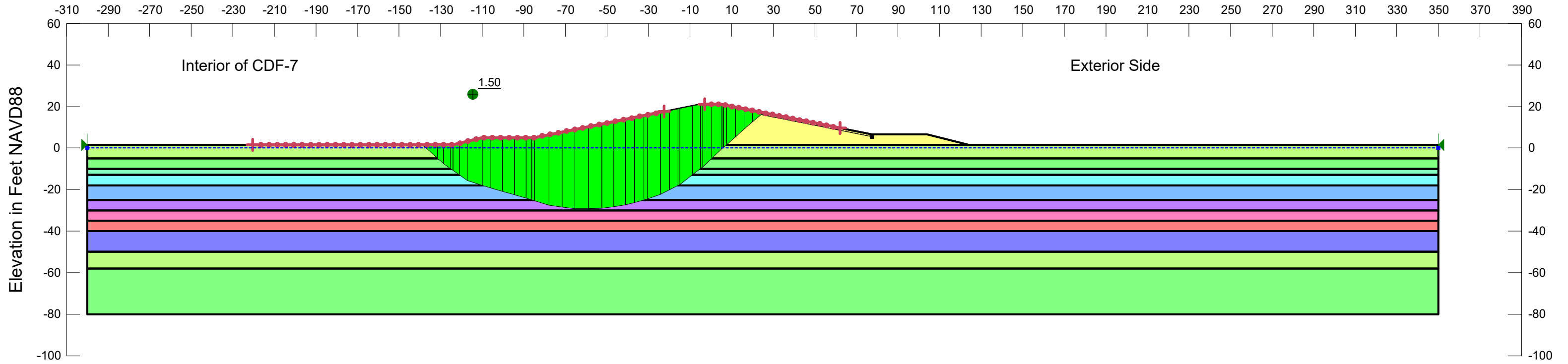
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**US Army Corps  
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 New Orleans District  
 Upper Barataria Basin  
 Stability Analysis for Cost Estimate  
 Alternative 6

Top of Levee - Entry Exit Slip Surface  
 Louisiana



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 Page 45/49

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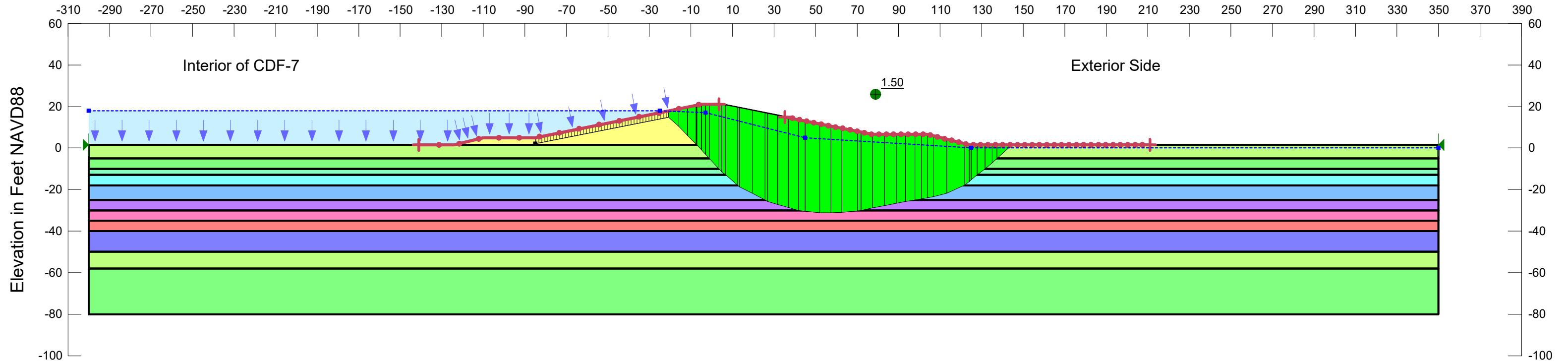
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**US Army Corps  
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 New Orleans District  
 Upper Barataria Basin  
 Stability Analysis for Cost Estimate  
 Alternative 6

Low Water Level - Entry Exit Slip Surface  
 Louisiana



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 Page 45/49

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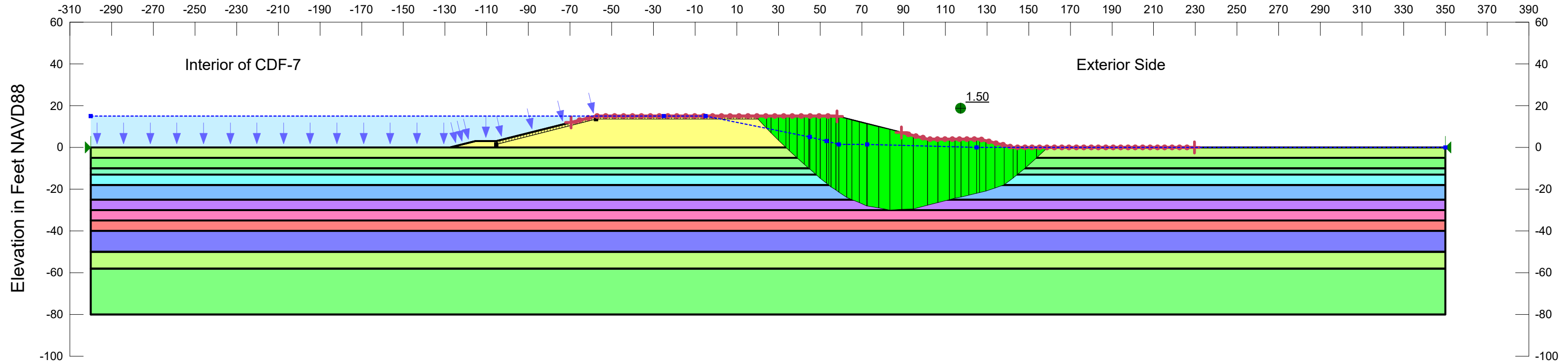
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**US Army Corps  
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 New Orleans District  
 Upper Barataria Basin  
 Stability Analysis for Cost Estimate  
 Alternative 6

Still Water Level - Entry Exit Slip Surface  
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 Page 45/49

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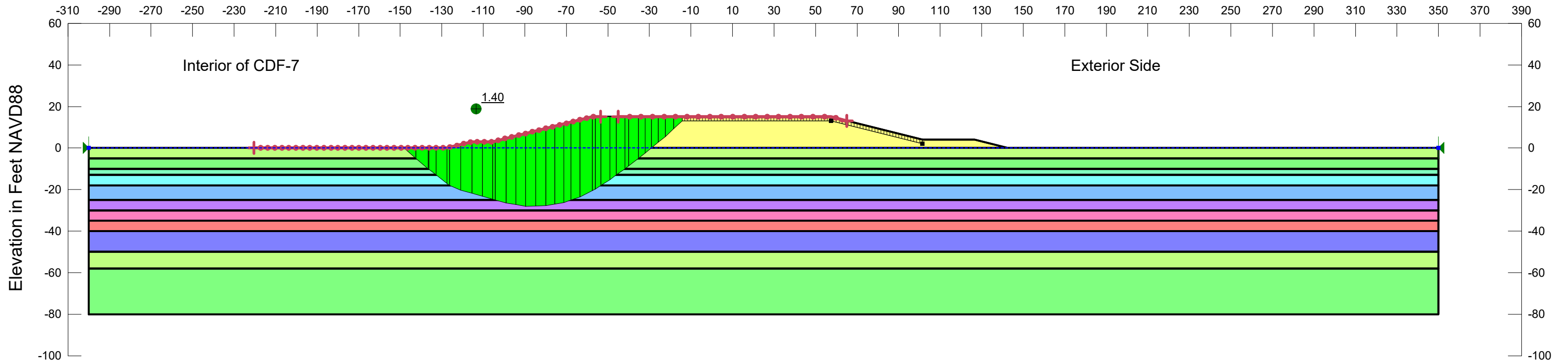


**US Army Corps  
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 New Orleans District  
 Upper Barataria Basin  
 Stability Analysis for Cost Estimate  
 Alternative 6

Top of Levee - Entry Exit Slip Surface  
 Louisiana

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 Page 45/49

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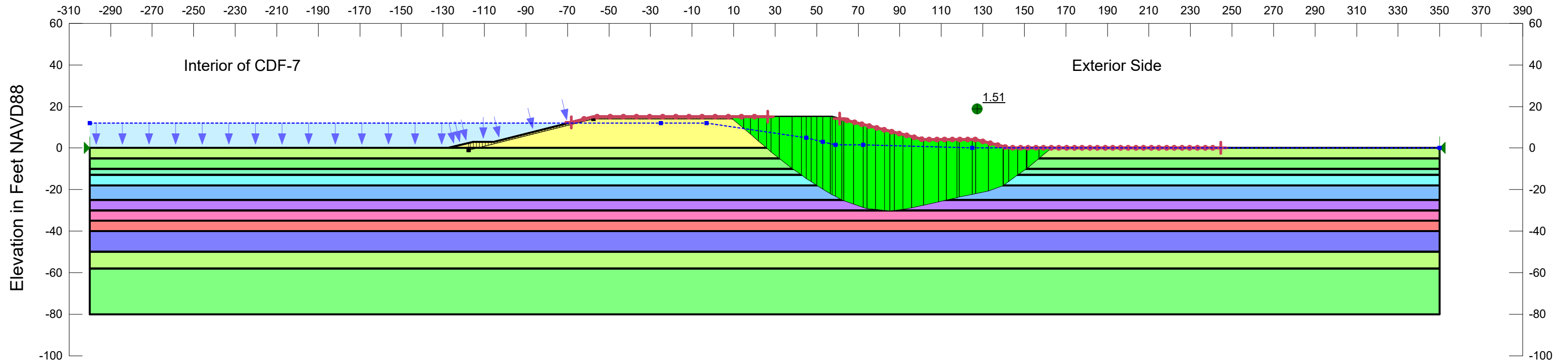
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Low Water Level - Entry Exit Slip Surface  
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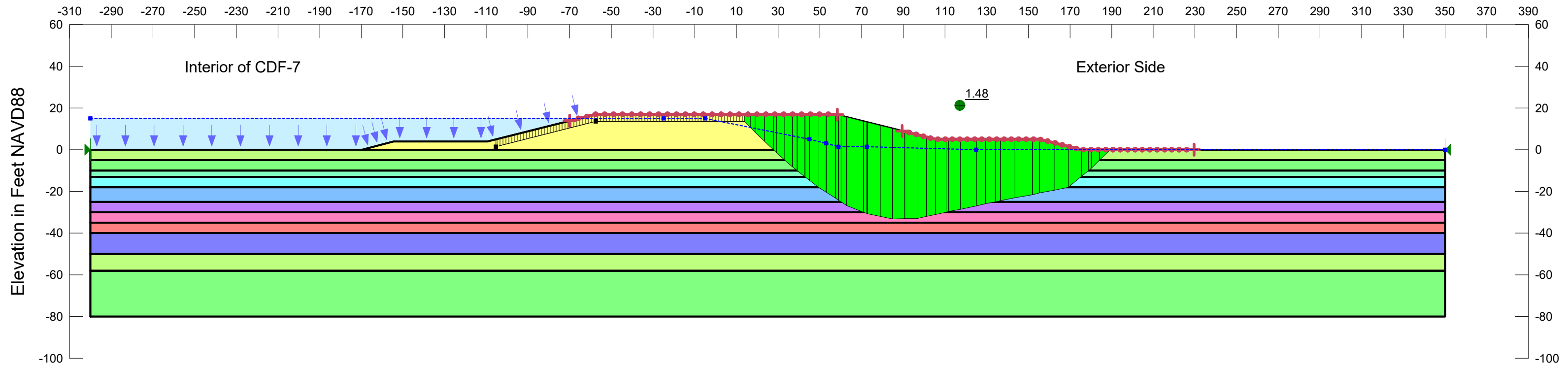
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**US Army Corps  
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 New Orleans District  
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 Alternative 6

Still Water Level - Entry Exit Slip Surface  
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 Page 45/49

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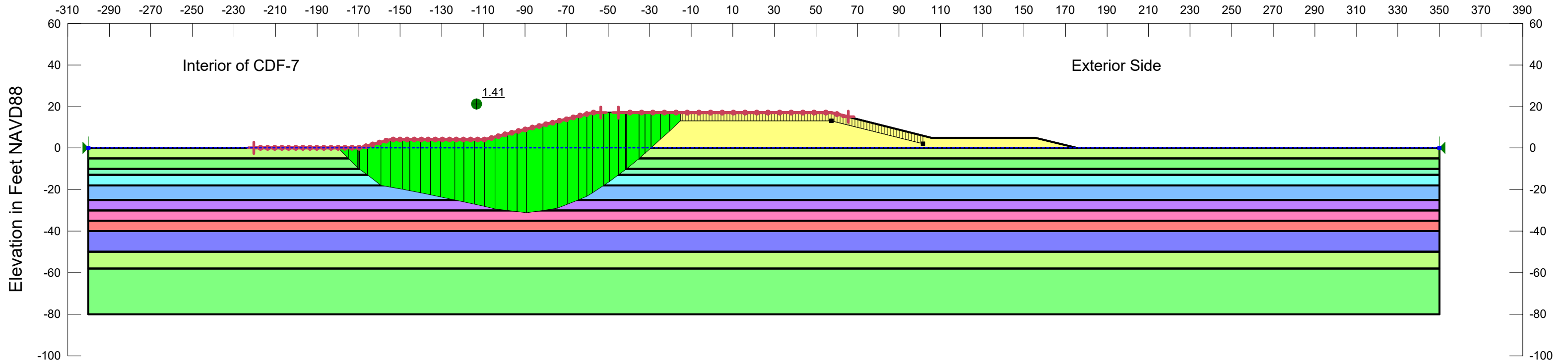
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**US Army Corps  
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 New Orleans District  
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 Stability Analysis for Cost Estimate  
 Alternative 8

Top of Levee - Entry Exit Slip Surface  
 Louisiana

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 Page 45/49

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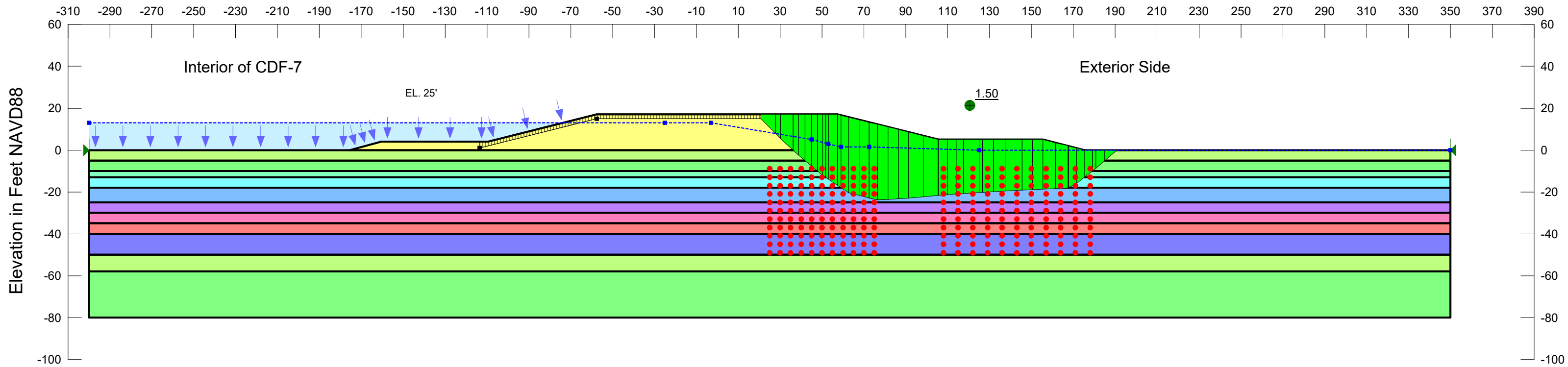
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 New Orleans District  
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 Alternative 8

Low Water Level - Entry Exit Slip Surface  
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Uses soil Properties from Magnolia Ridge Geotechnical Report  
 22557-SCP-Magnolia Ridge Levee Project - Report I - Earthen Levees - Report and Figures. pdf  
 Page 45/49

Gains in Strength from additional loadings were added for this stability analysis

GENERAL NOTES

CLASSIFICATION STRATIFICATION  
 SHEAR STRENGTHS AND UNIT WEIGHTS OF  
 THE SOIL WERE BASED ON THE RESULTS OF  
 UNDISTURBED BORINGS. SEE  
 BORING DATA PLATES.

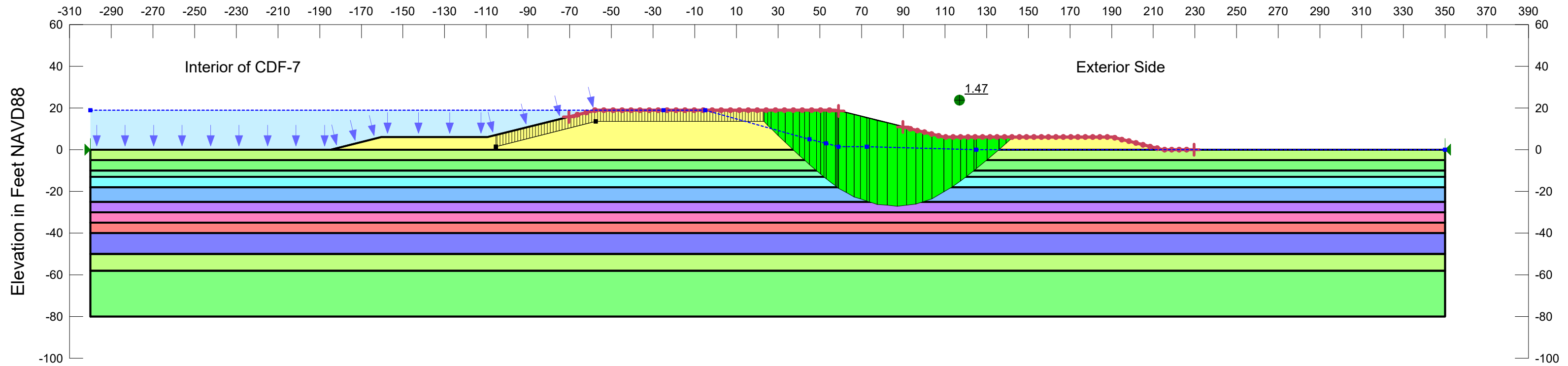
SHEAR STRENGTHS BETWEEN VERTICALS  
 WERE ASSUMED TO VARY LINEARLY BETWEEN  
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**US Army Corps  
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 New Orleans District  
 Upper Barataria Basin  
 Stability Analysis for Cost Estimate  
 Alternative 8

Still Water Level - Block Slip Surface  
 Louisiana

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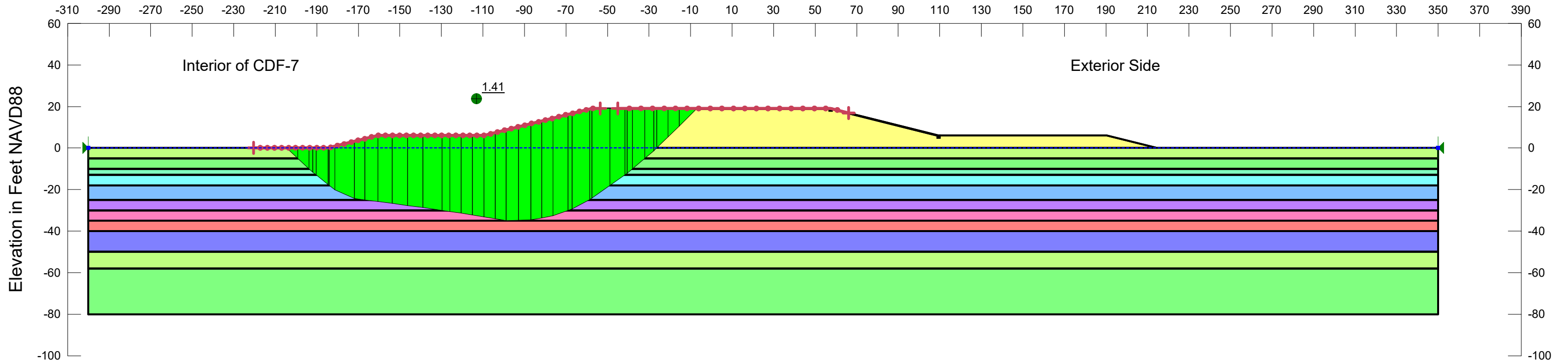
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Top of Levee - Entry Exit Slip Surface  
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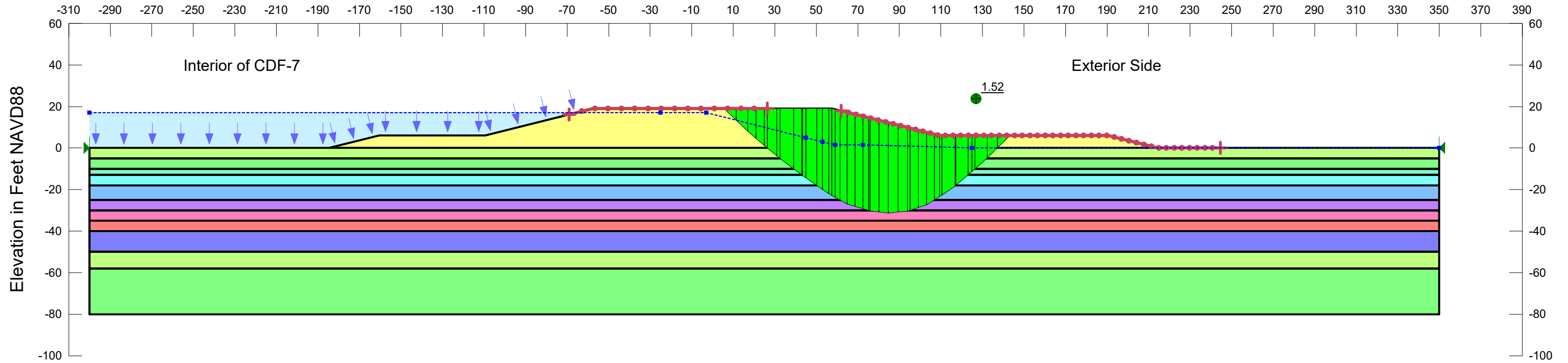
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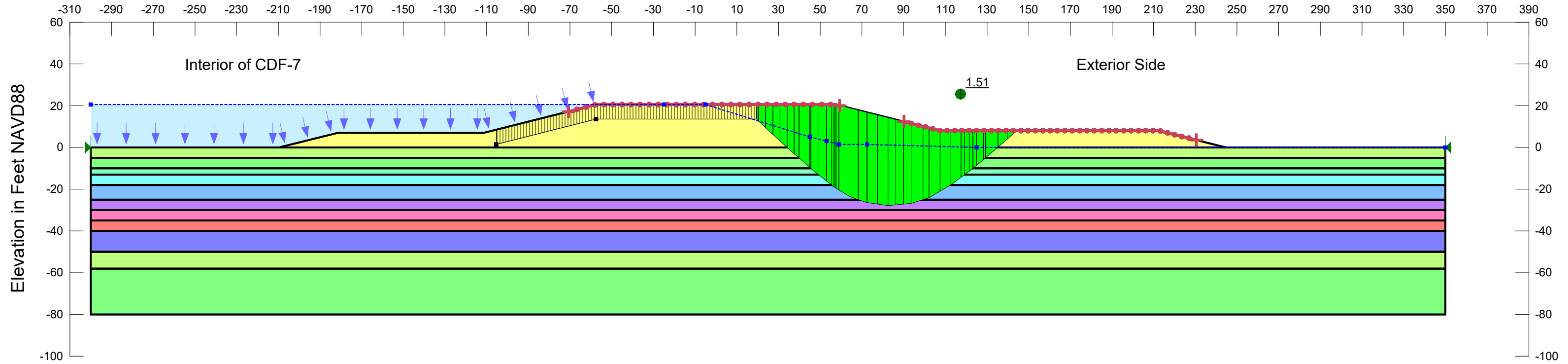


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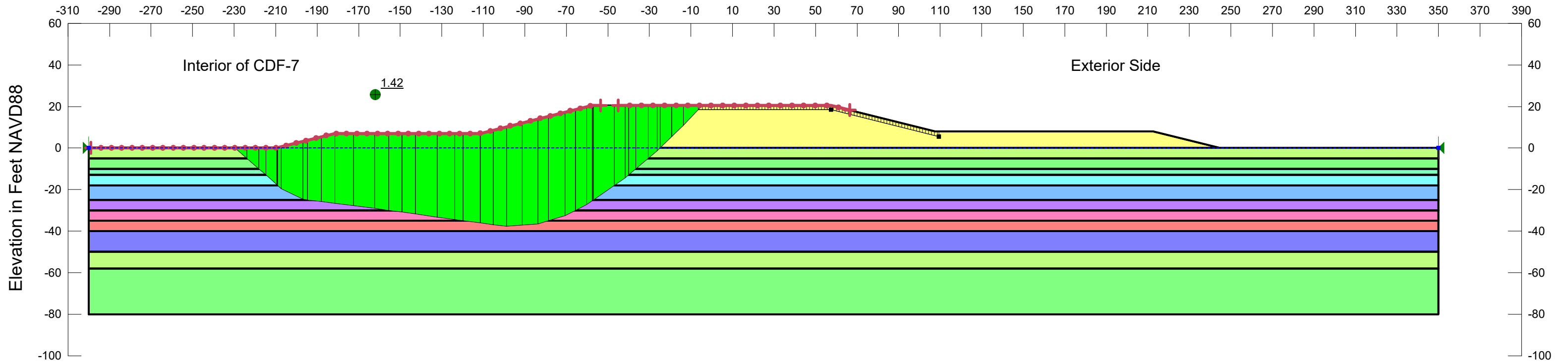
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 22557-SCP-Magnolia Ridge Levee Project - Report I - Earthen Levees - Report and Figures. pdf  
 Page 45/49

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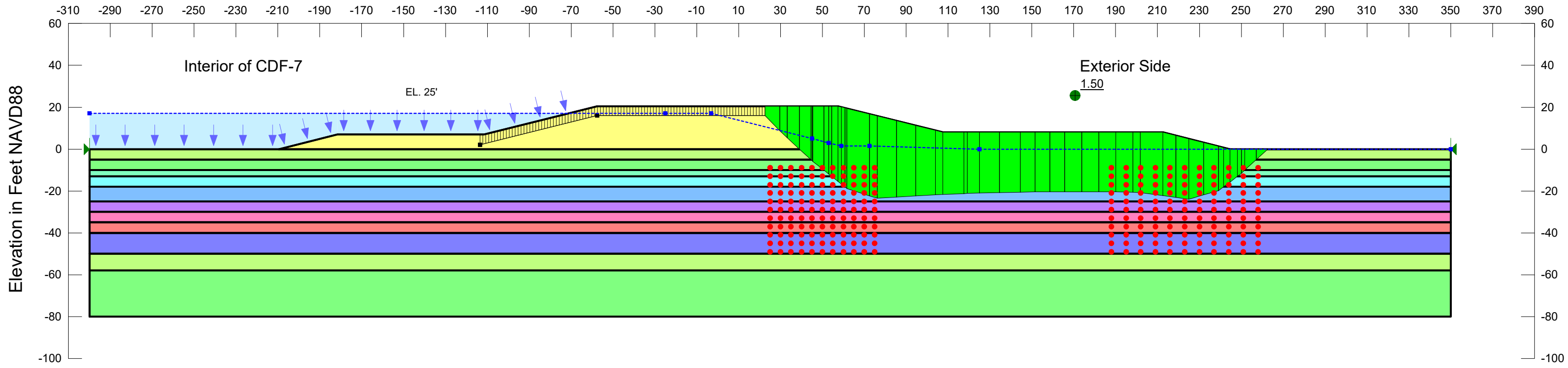
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